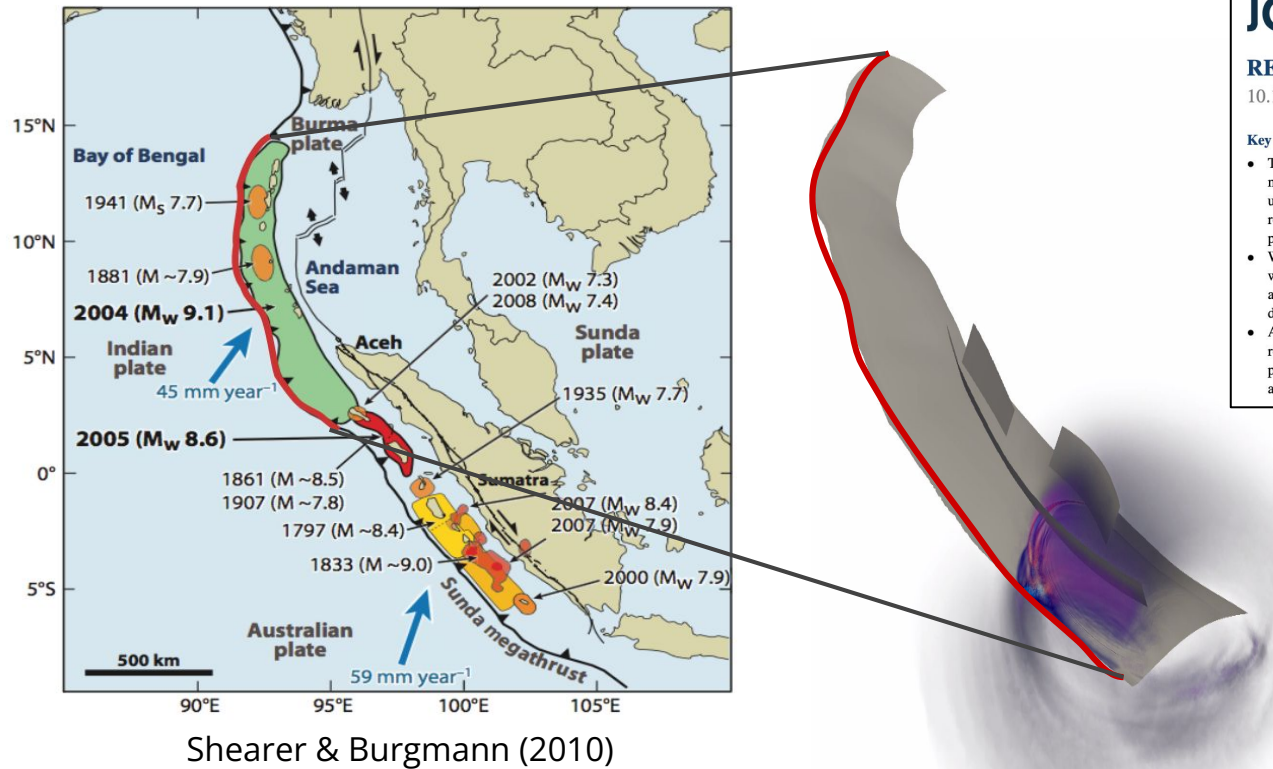


# Energy budget analyses of scenario earthquake ruptures at Cascadia

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## JGR Solid Earth

RESEARCH ARTICLE  
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### The State of Pore Fluid Pressure and 3-D Megathrust Earthquake Dynamics

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**Abstract** We study the effects of pore fluid pressure ( $P_f$ ) on the pre-earthquake, near-fault stress state, and 3-D earthquake rupture dynamics through six scenarios utilizing a structural model based on the 2004  $M_w$  9.1 Sumatra-Andaman earthquake. As pre-earthquake  $P_f$  magnitude increases, effective normal stress and fault shear strength decrease. As a result, magnitude, slip, peak slip rate, stress drop, and rupture velocity of the scenario earthquakes decrease. Comparison of results with observations of the 2004 earthquake support

**Key Points:**

- Three-dimensional dynamic rupture modeling of megathrust earthquakes under varying pore fluid conditions reveal very high pre-earthquake fluid pressure
- When pore fluid pressure increases with the lithostatic gradient, peak slip and peak slip rate occur at shallower depths, controlling hazard
- Apparent co-seismic principal stress rotations and heterogeneous absolute post-seismic stress states reflect aftershock focal mechanisms



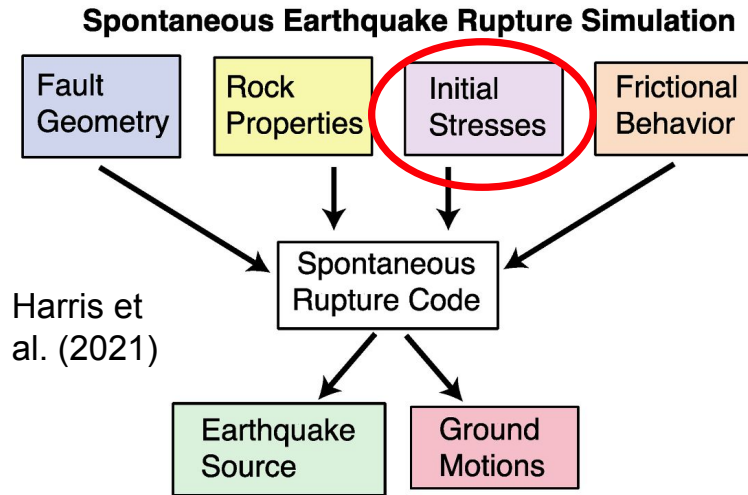
Lindsay Gross (Twinning Mentee 2024-25)

Sean Hsieh (MS, Computer Science)

Corey Liscombe (SJSU Undergraduate Research Opportunity Program)



# 4 models with high or very high co-seismic pore fluid pressure (Pf) and lithostatic or sub-lithostatic Pf gradient

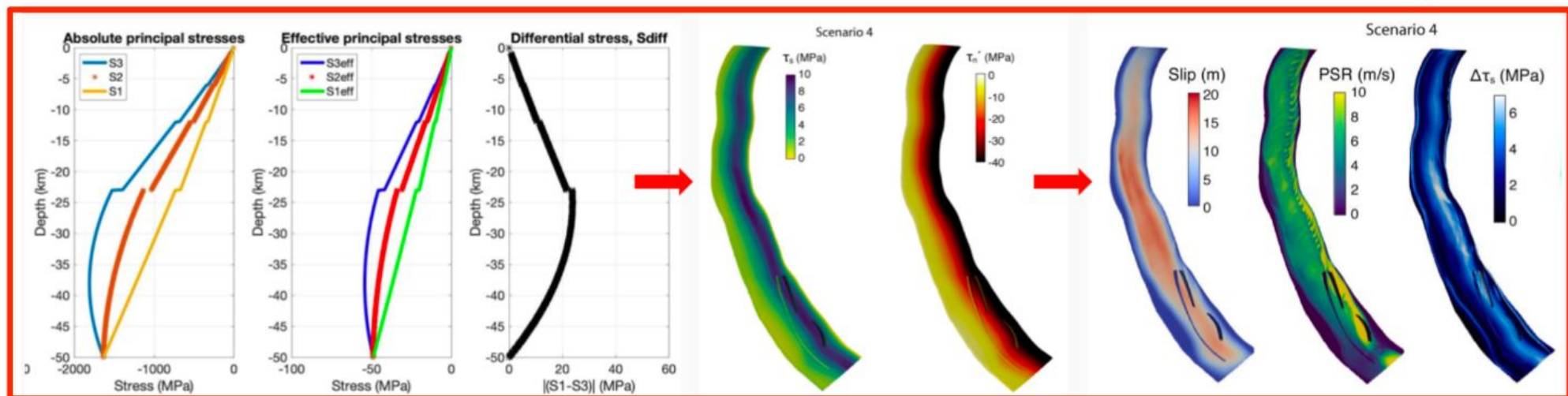


**Table 2**  
*Initial Conditions for All Scenarios*

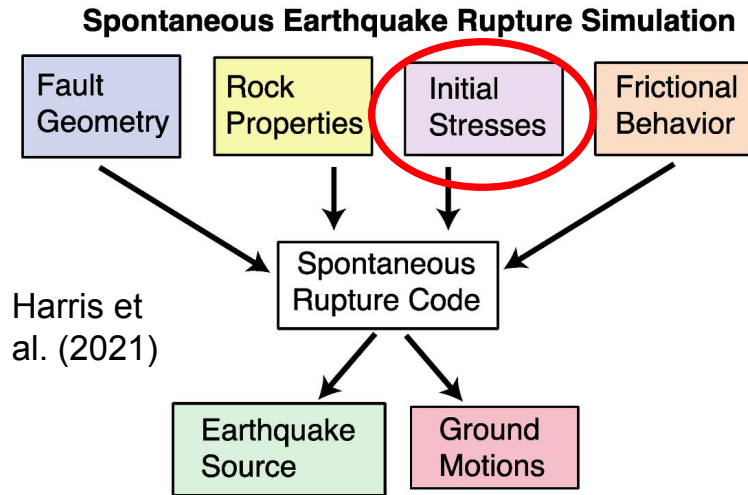
Scenario	$P_f$ level (% of $\sigma_v$ <sup>a</sup> )	$P_f$ parameterization
3	High (93%)	$0.93\sigma_v$
4	Very high (97%)	$0.97\sigma_v$
5	High (93%)	$\sigma_v - 42$ MPa
6	Very high (97%)	$\sigma_v - 20$ MPa

*Earthquake Characteristics Averaged Across the Megathrust*

Scenario	$M_w$	Mean slip (m) <sup>a</sup>	Mean PSR (m/s) <sup>b</sup>	Mean $\Delta\tau_s$ (MPa) <sup>c</sup>	Mean $V_r$ (m/s) <sup>d</sup>
4	9.0	8	5	3	2,370



# 4 models with high or very high co-seismic pore fluid pressure (Pf) and lithostatic or sub-lithostatic Pf gradient

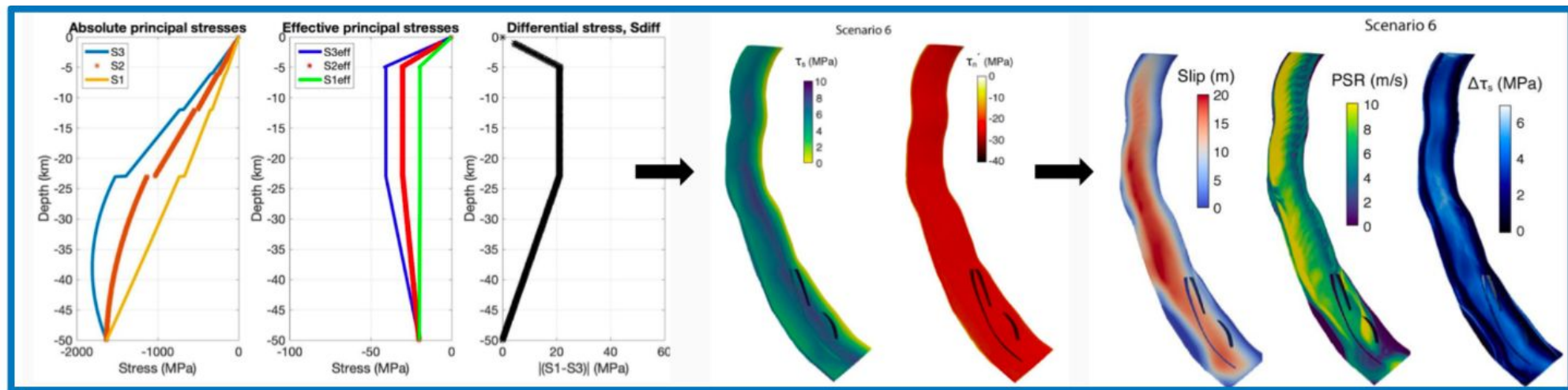


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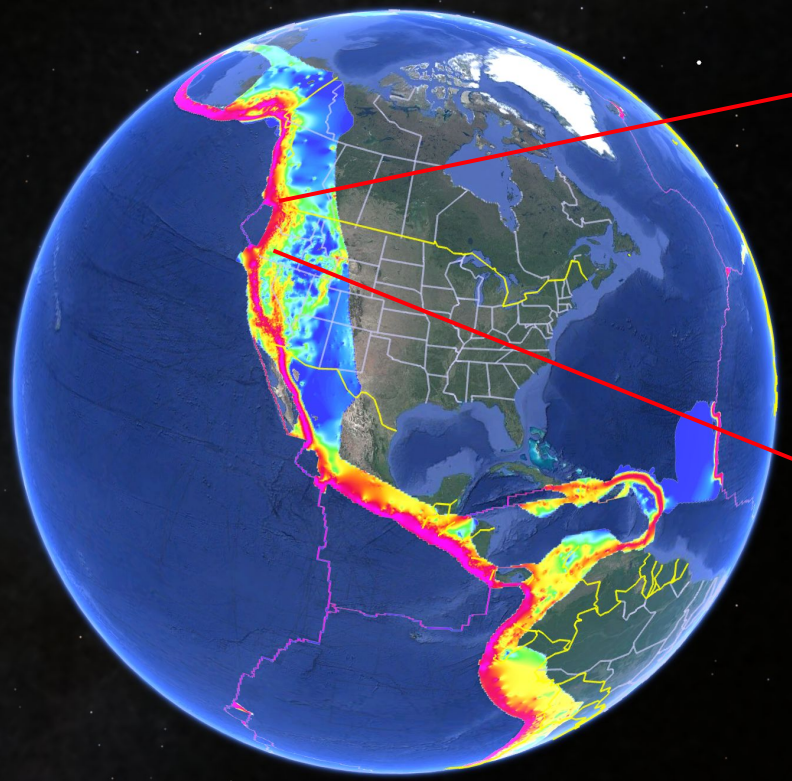
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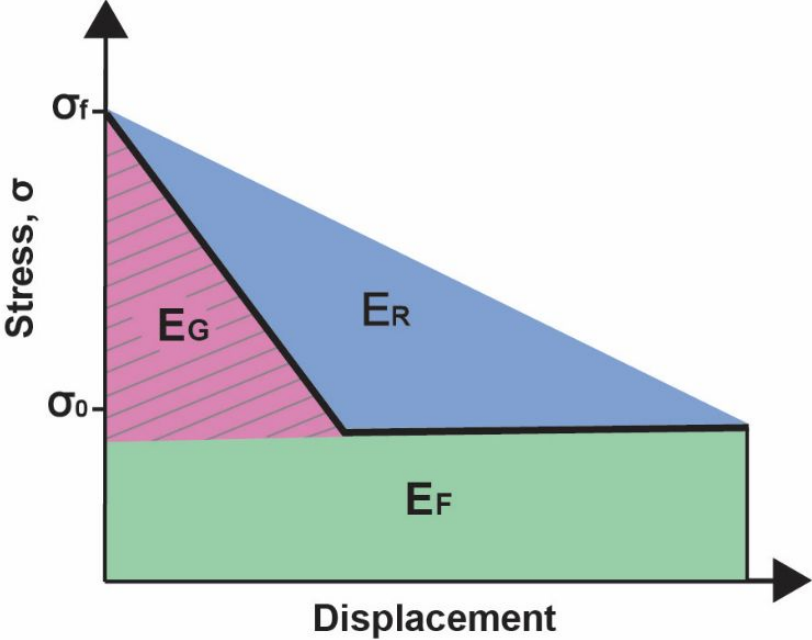
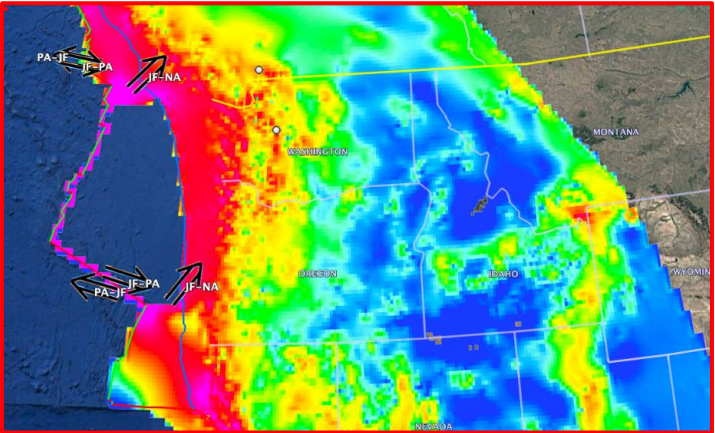
Scenario	$M_w$	Mean slip (m) <sup>a</sup>	Mean PSR (m/s) <sup>b</sup>	Mean $\Delta\tau_s$ (MPa) <sup>c</sup>	Mean $V_r$ (m/s) <sup>d</sup>
4	9.0	8	5	3	2,370
6	9.1	10	6	3	2,624



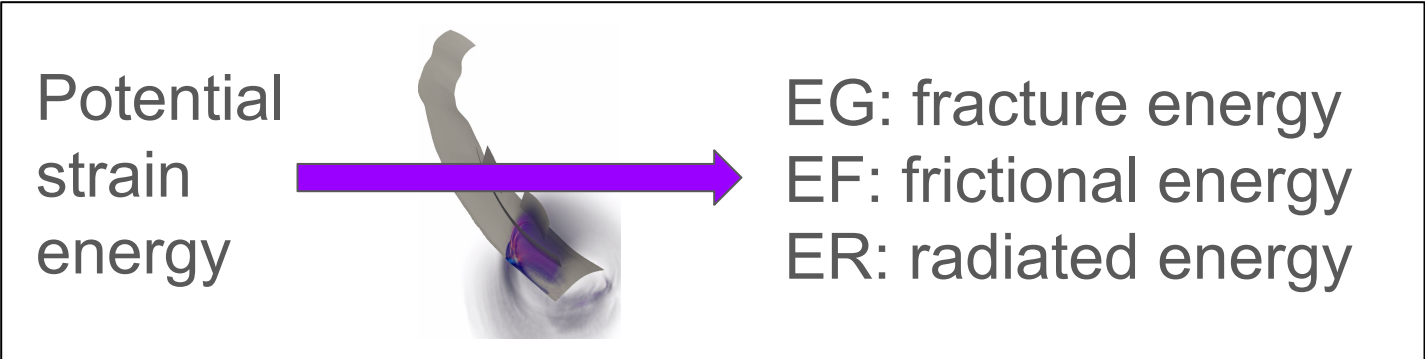
# Earthquake energy budget



Global crustal strain rate model from horizontal geodetic data (v.2.1) (Kreemer et al., 2014)

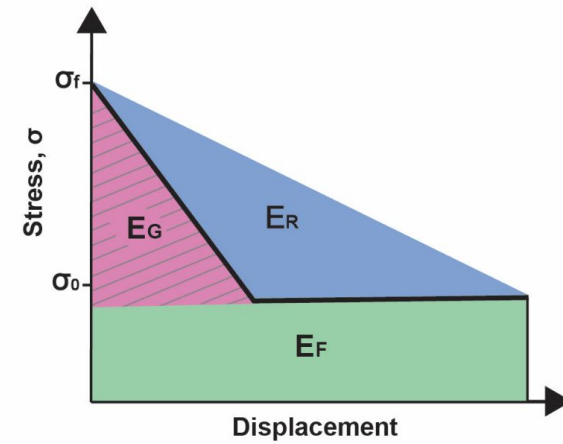
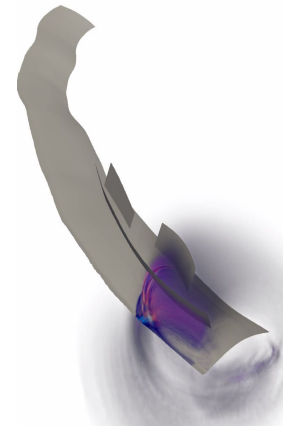


(Coffey et al., 2023)



# Earthquake energy budget

$$W_{\text{total}} = \int_{\Sigma} \sigma_0(\xi) \cdot \Delta \mathbf{u}_1(\xi) d\Sigma - \int_0^{\infty} \int_{\Sigma} \sigma(\xi, t) \cdot \Delta \mathbf{v}(\xi, t) d\Sigma dt$$



(Coffey et al., 2023)

EG: fracture energy  
EF: frictional energy



$$W_{\text{static}} = \frac{1}{2} \int_{\Sigma} [\sigma_0(\xi) - \sigma_1(\xi)] \cdot \Delta \mathbf{u}_1(\xi) d\Sigma$$

ER: radiated energy

$$E_R = W_{\text{total}} - W_{\text{static}} = \int_{\Sigma} \frac{\sigma_0(\xi) + \sigma_1(\xi)}{2} \cdot \Delta \mathbf{u}_1(\xi) d\Sigma - \int_0^{\infty} \int_{\Sigma} \sigma(\xi, t) \cdot \Delta \mathbf{v}(\xi, t) d\Sigma dt.$$

W = work

$\Sigma$  = fault surface

$\Delta \mathbf{u}_1$  = final slip

$\Delta \mathbf{v}$  = slip velocity

t = time

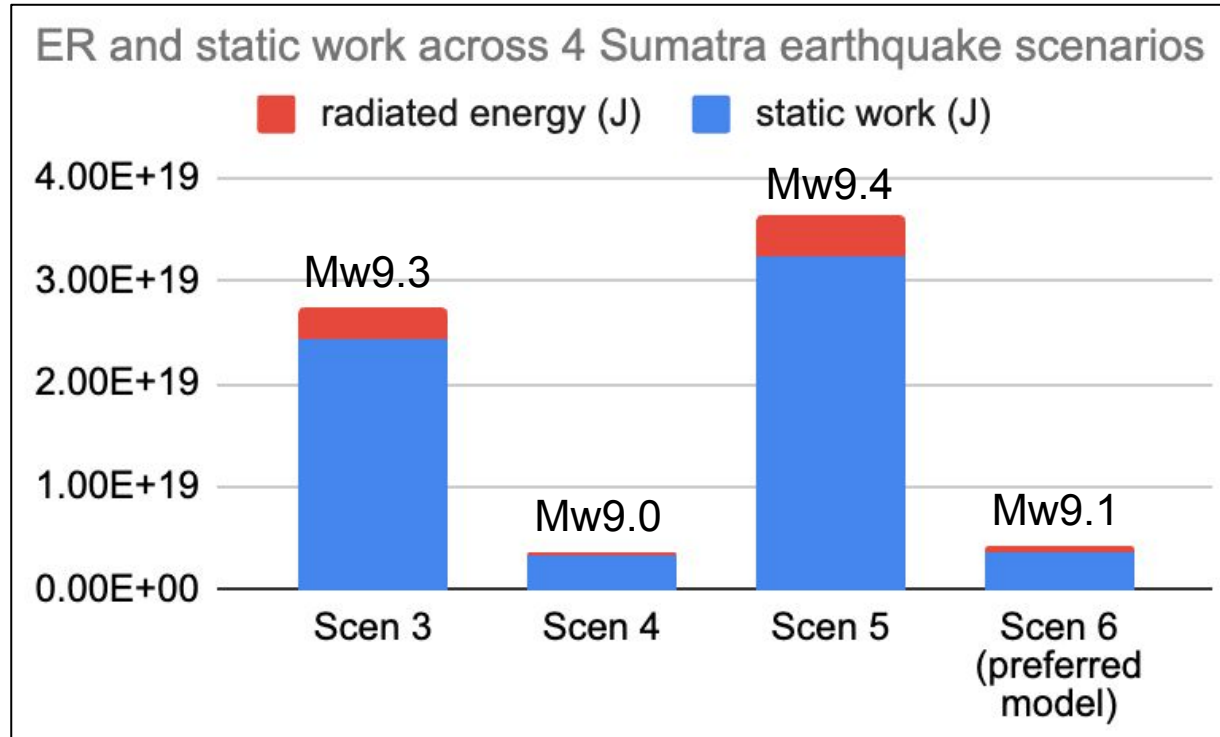
$\sigma_0$  = initial shear stress

$\sigma$  = shear stress

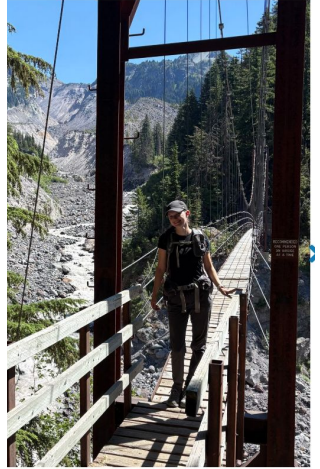
$\sigma_1$  = final shear stress

Ma & Archuleta (2006)

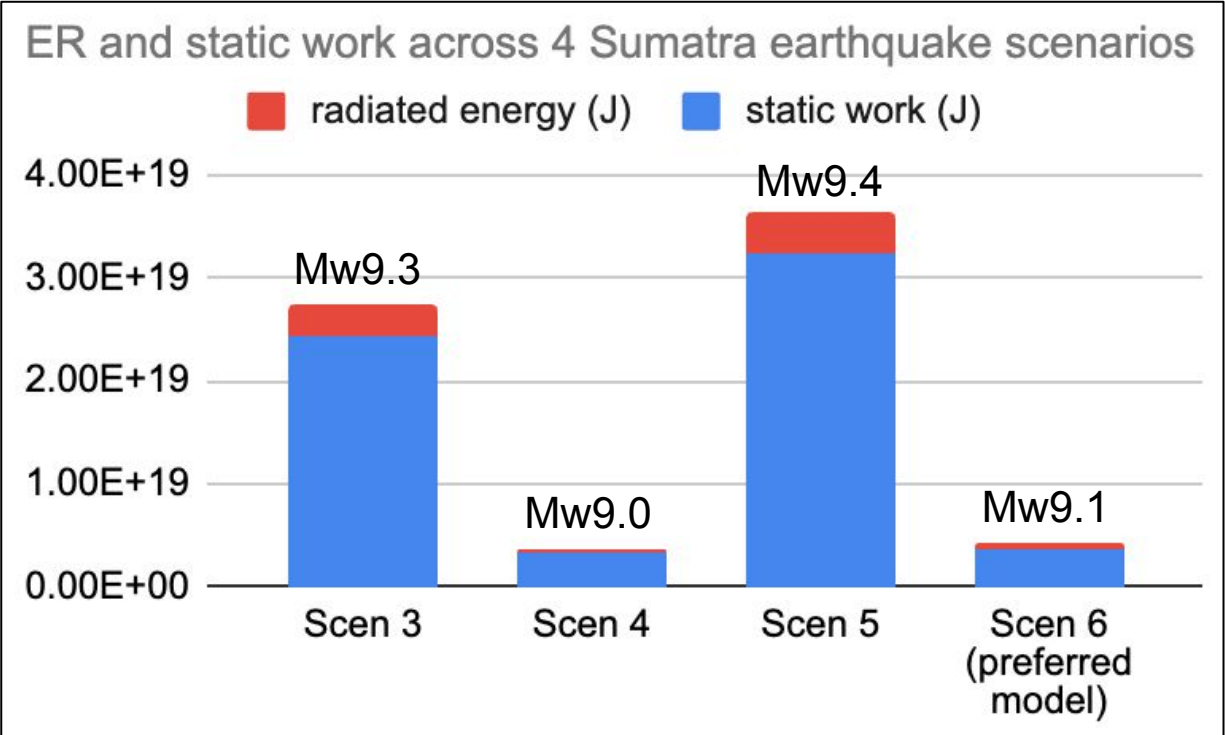
# Energy budgets for 2004 Sumatra earthquake models



- Total energy scales with magnitude



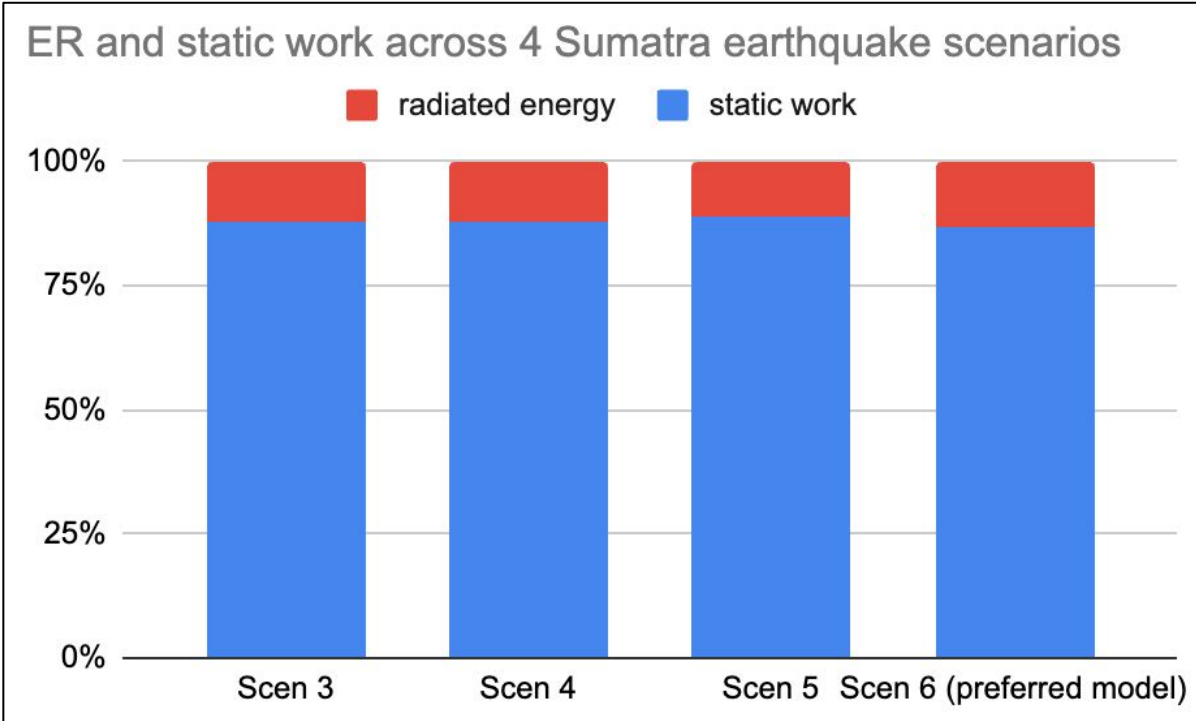
# Energy budgets for 2004 Sumatra earthquake models



- Total energy scales with magnitude



- All 4 earthquake models have the same energy budget

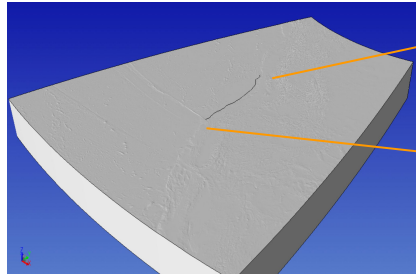
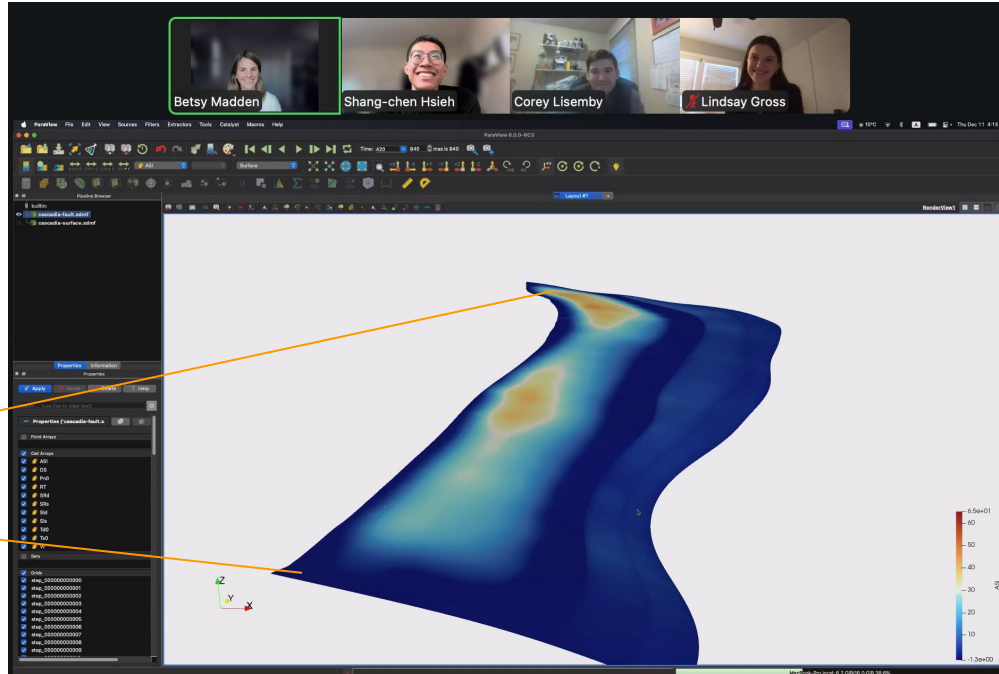
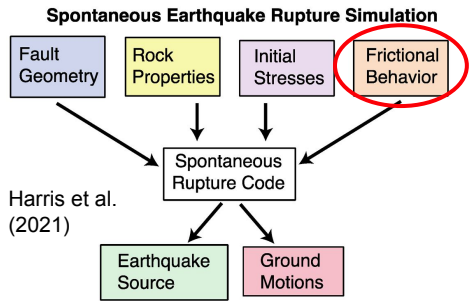


# Energy budget for 2004 Sumatra earthquake

- Models match ER in order of magnitude, but are almost twice as high
- High ER results in low ER/M0

<b>Energy Component</b>	<b>Observations</b> (Kanamori, 2006, Table 1)	<b>Model - Sumatra Scenario 6</b>
<b>Mw</b>	9.1	9.1
<b>Seismic Moment (M0)</b>	<b>6.5 E+22 J</b>	4.93 E+22 J
<b>Total Work (Wt)</b>	n/a	4.23 E+18 J
<b>Static Work (Ws)</b>	n/a	3.67 E+18 J
<b>ER = Wt-Ws</b>	3 E+17 J	<b>5.60 E+17 J</b>
<b>ER/M0</b>	4.6 E-6	<b>1.14 E-05</b>

# Cascadia scenario earthquake ruptures & energy budgets



	Observations - Sumatra	Model - Sumatra	Model - Cascadia
Mw	9.1	9.1	
Seismic Moment (M0)	6.5 E+22 J	4.93 E+22 J	
Total Work (Wt)	n/a	4.23 E+18 J	
Static Work (Ws)	n/a	3.67 E+18 J	
ER = Wt-Ws	3 E+17 J	5.60 E+17 J	
ER/M0	4.6 E-6	1.14 E-05	

Let  $\sigma_{ij}$  denote the stress tensor. Define:

$$\text{Mean stress } \sigma_m = \frac{1}{3}(\sigma_{11} + \sigma_{22} + \sigma_{33})$$

$$\text{Stress deviator } s_{ij} = \sigma_{ij} - \sigma_m \delta_{ij}$$

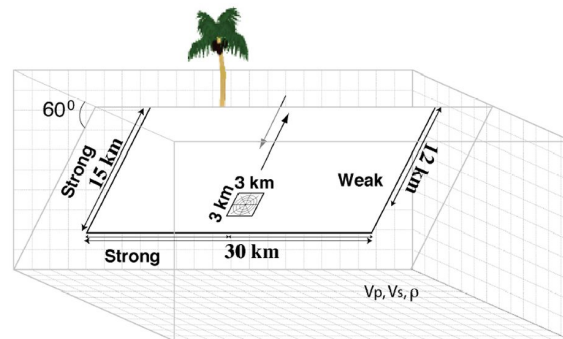
$$\text{Second invariant of the stress deviator } J_2(\sigma) = \frac{1}{2} \sum_{i,j} s_{ij} s_{ji}$$

$$\text{Drucker-Prager yield stress } Y(\sigma) = \max(0, c \cos \phi - (\sigma_m + P_f) \sin \phi)$$

$$\text{Drucker-Prager yield function } F(\sigma) = \sqrt{J_2(\sigma)} - Y(\sigma)$$

The Drucker-Prager material is required to satisfy the yield equation:  $F(\sigma) \leq 0$

When  $F(\sigma) < 0$ , the material behaves like a linear elastic material, with Lamé parameters  $\lambda$  and  $\mu$ .



Harris et al. (2018)

→ Add off-fault plasticity

→ Evaluate different megathrust interface geometries Elston et al. (2025)

