

Estimating tsunami risk

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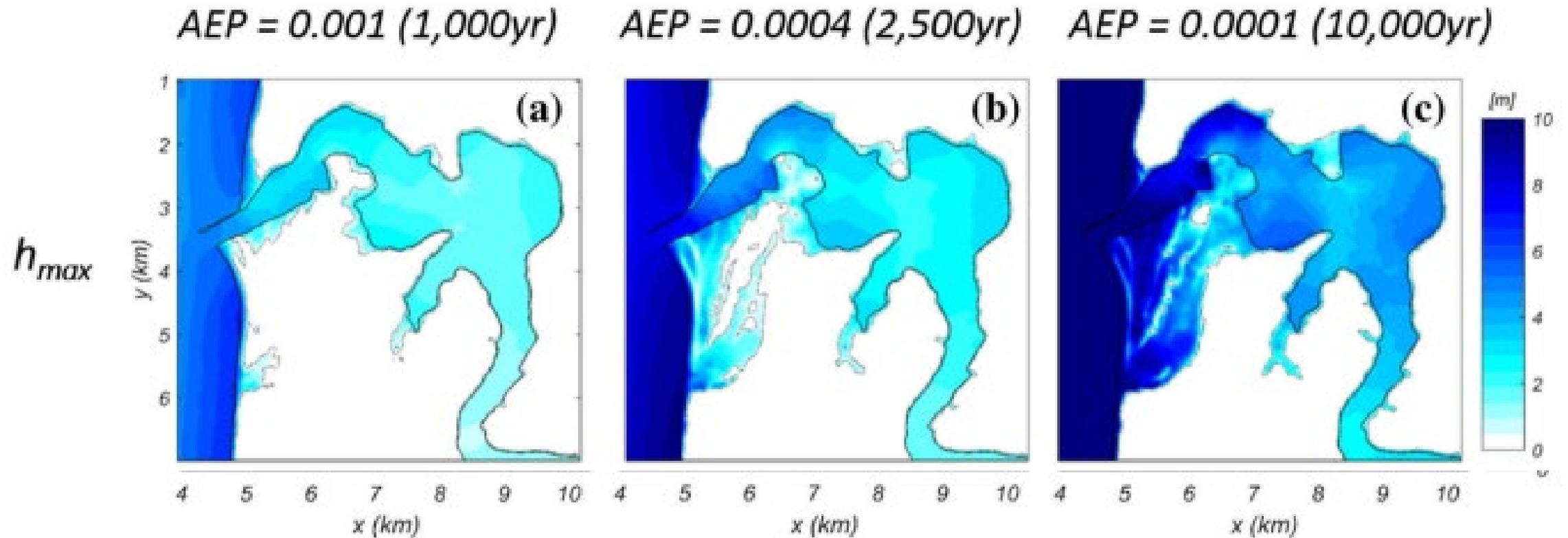
Hyoungsu Park

Dylan Sanderson

Kameshwar Sabarethinam



Oregon State
University



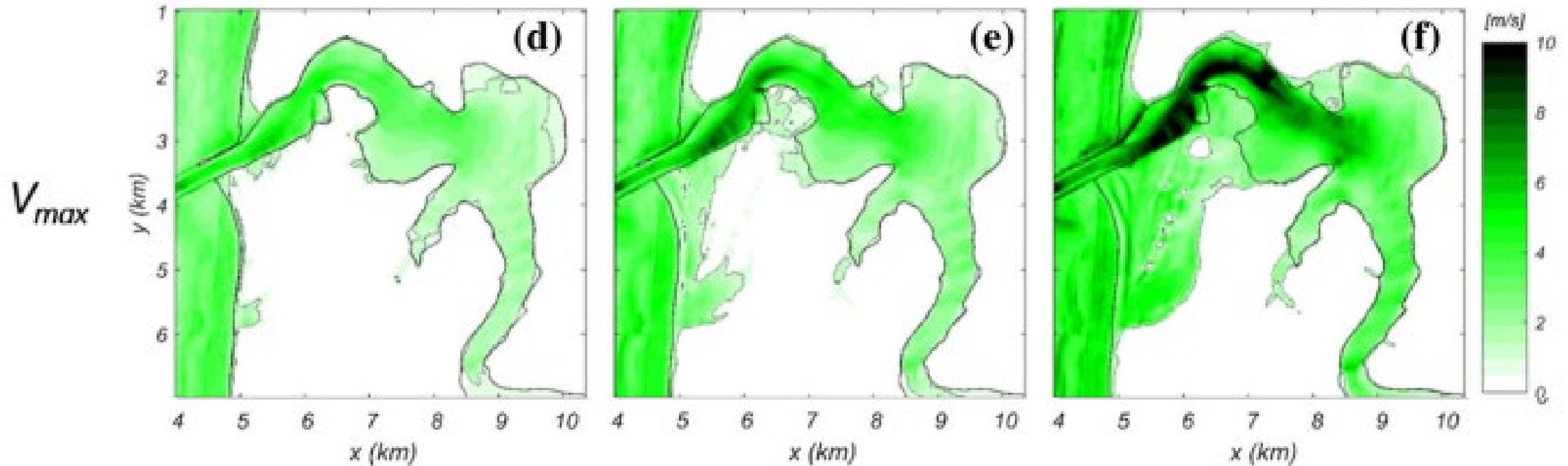
Flow Depth

Park H, DT Cox, AR Barbosa (2018)
 "Probabilistic Tsunami Hazard Assessment
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 Community," *Natural Hazards*,
<https://doi.org/10.1007/s11069-018-3460-3>.

$AEP = 0.001$ (1,000yr)

$AEP = 0.0004$ (2,500yr)

$AEP = 0.0001$ (10,000yr)



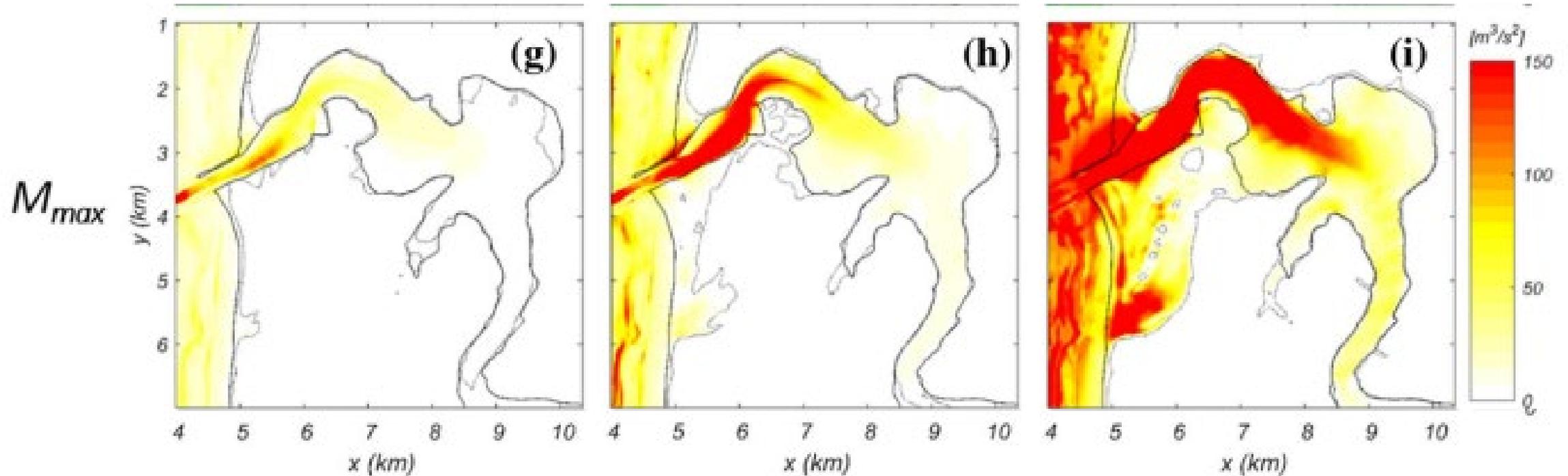
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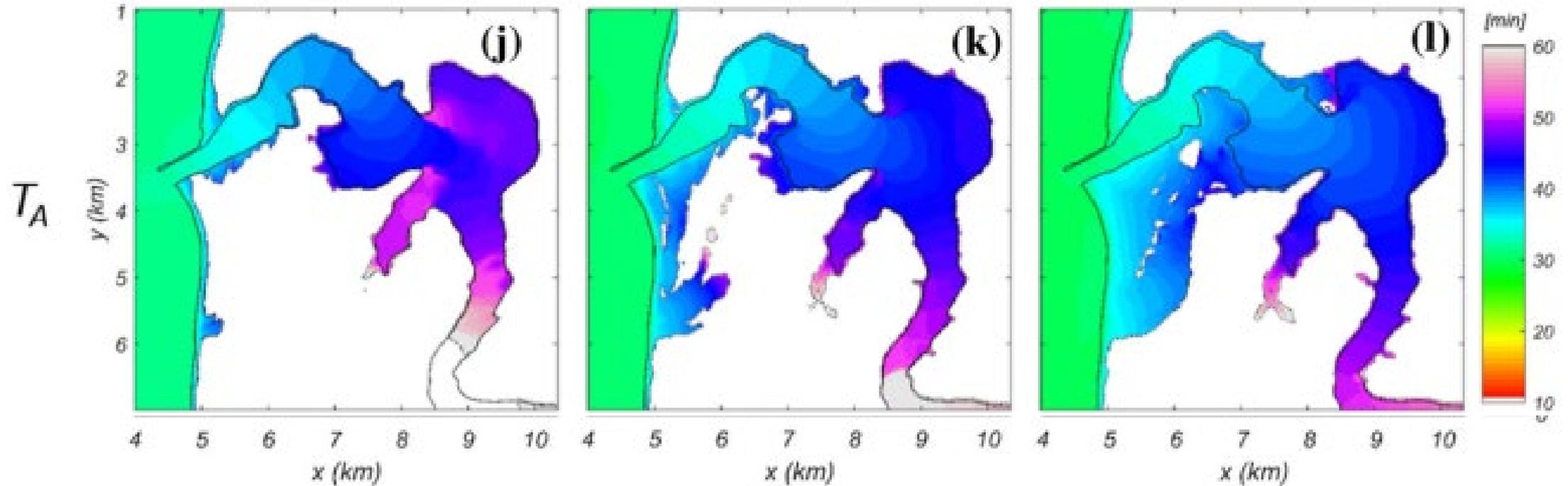
Momentum Flux

Park H, DT Cox, AR Barbosa (2018)
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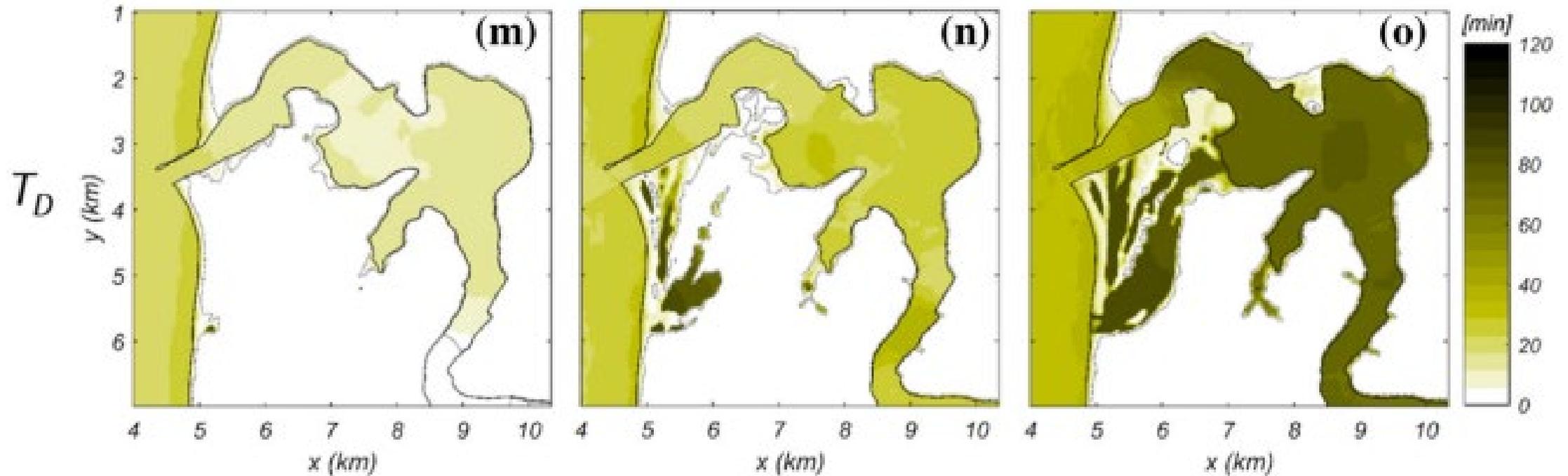
Arrival Time

Park H, DT Cox, AR Barbosa (2018)
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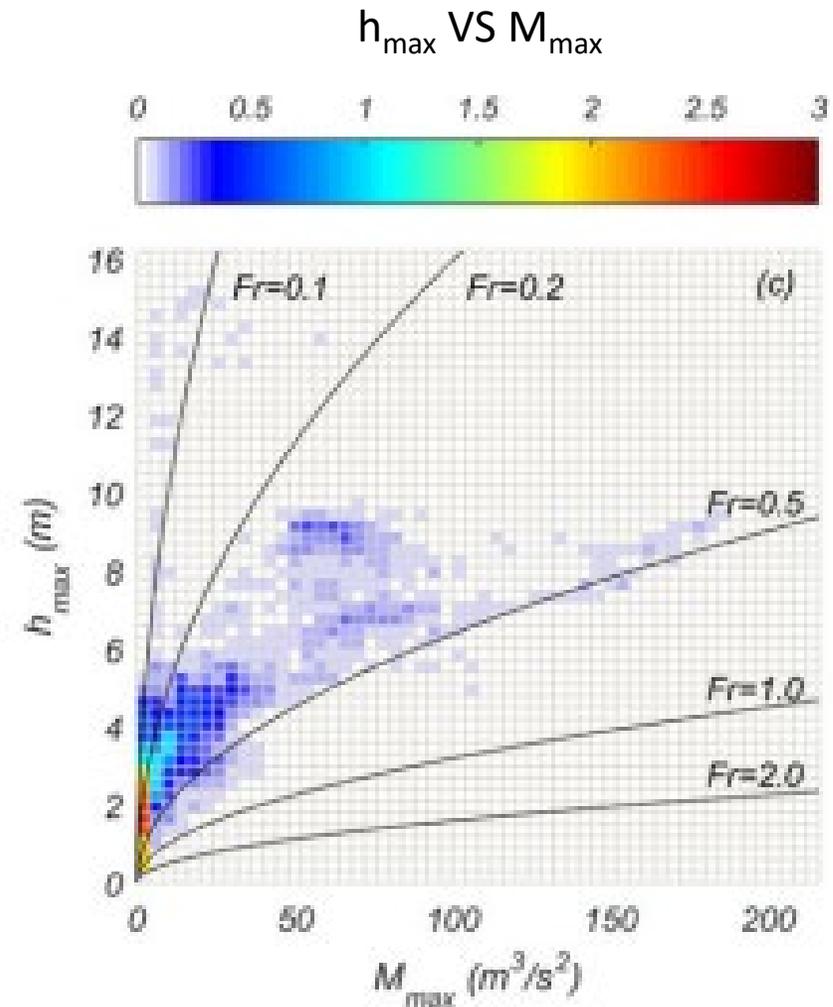
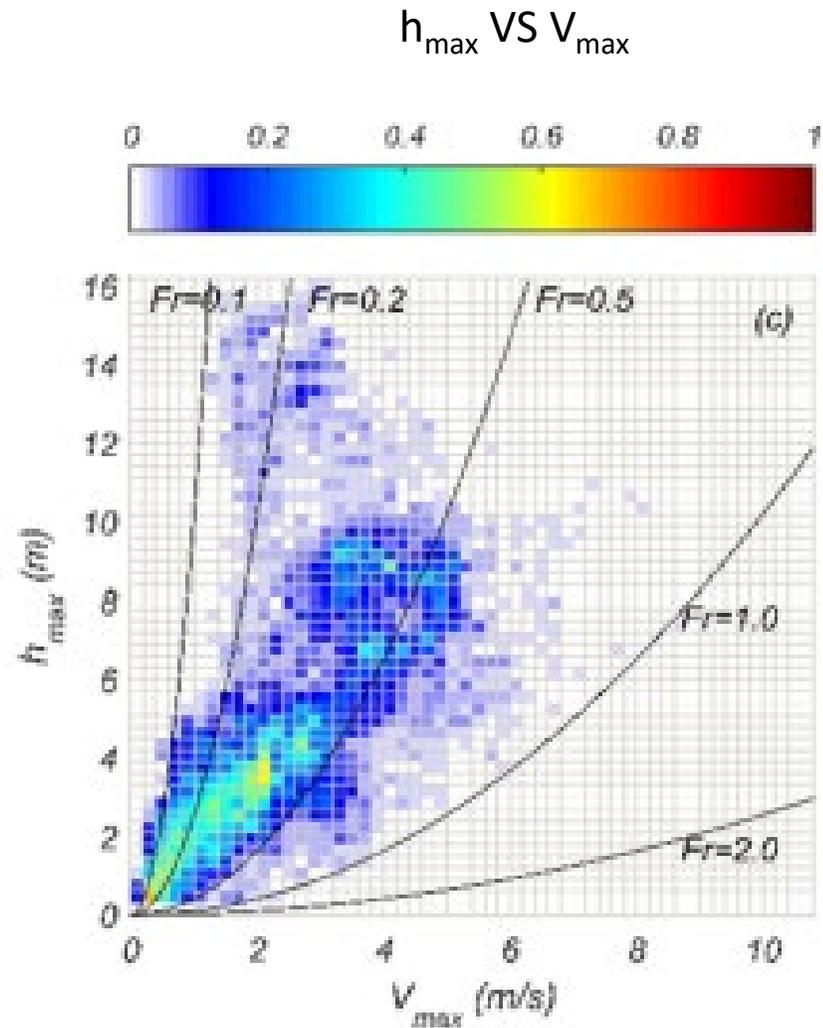


Duration of Flooding

Park H, DT Cox, AR Barbosa (2018)
“Probabilistic Tsunami Hazard Assessment
(PTHA) for Resilience Assessment of a Coastal
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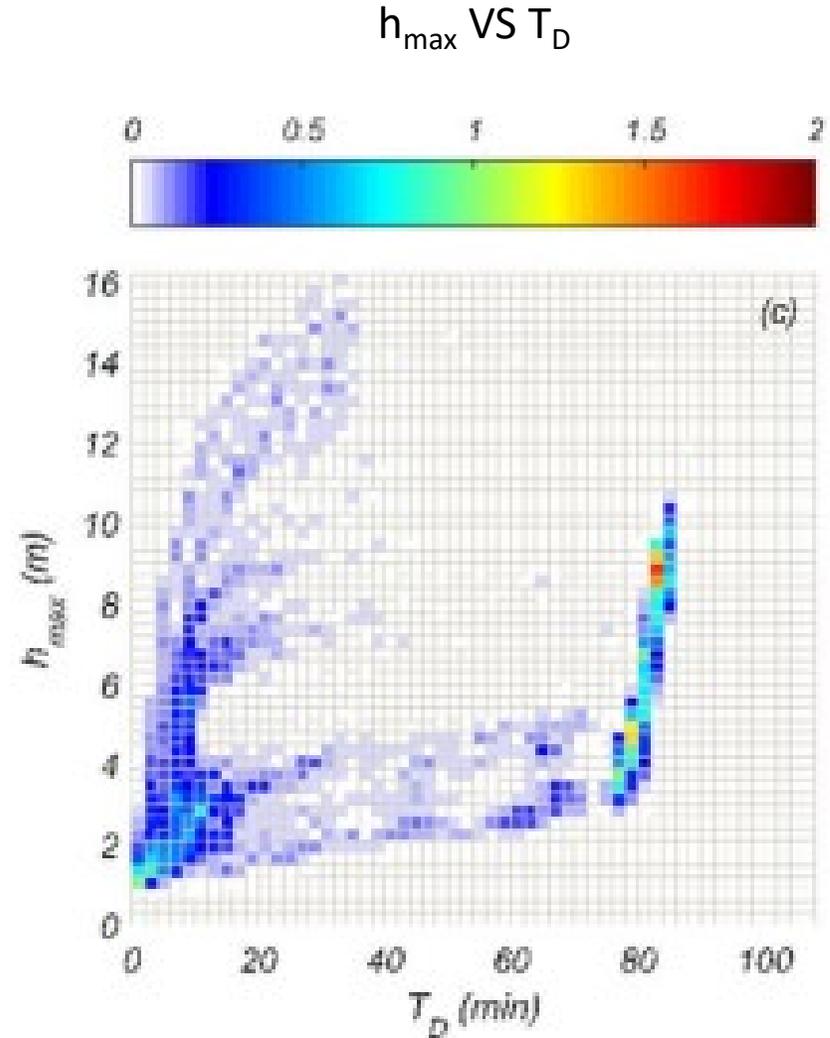
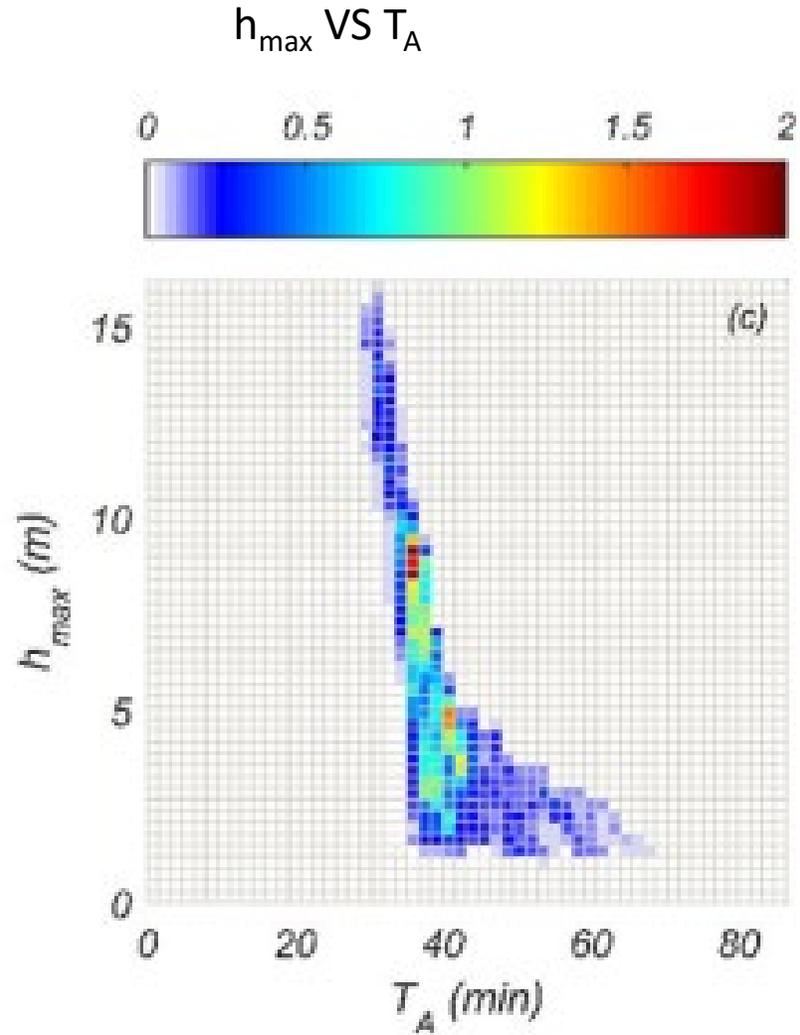
Joint Distributions of IMs

Correlation or relationship among h_{\max} and other IMs



Joint Distributions of IMs

- Correlation or relationship among h_{\max} and other IMs



PTHA Comparison for Newport, Oregon

Park et al., 2018

ASCE 7-16

DOGAMI "M"

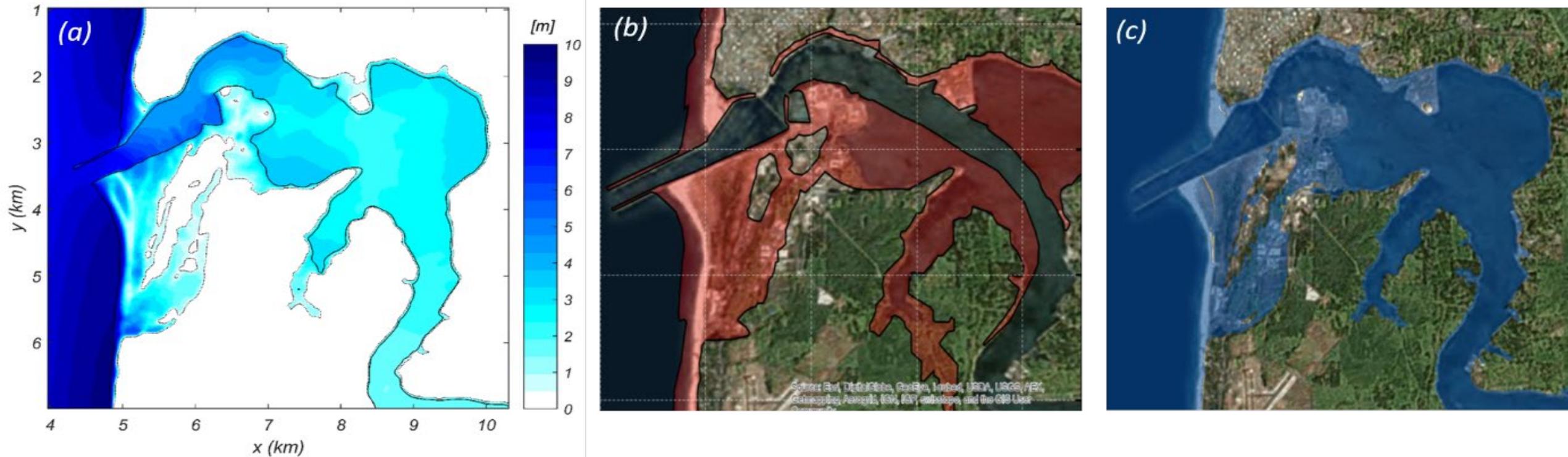
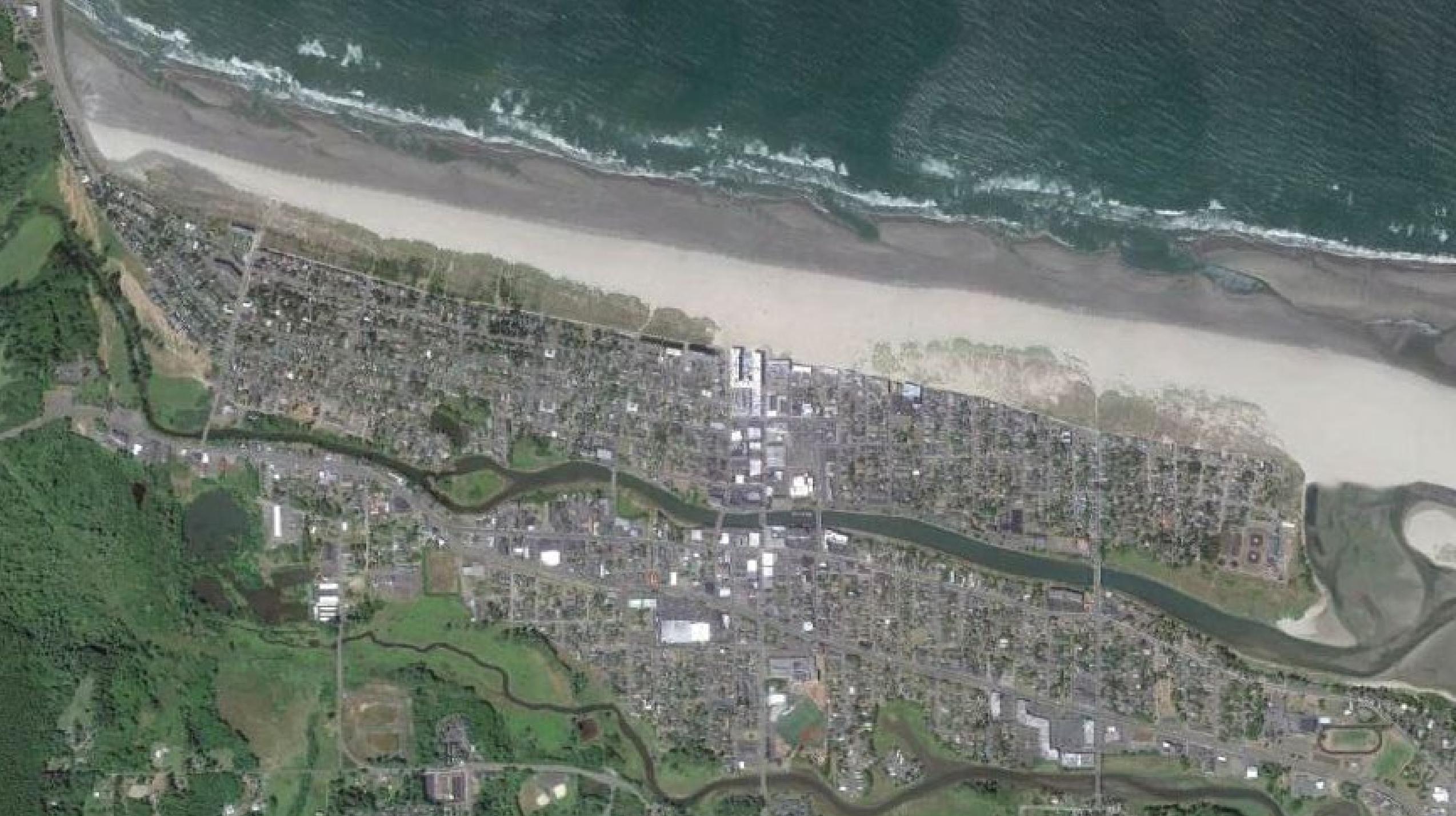


Figure 7: Comparison of maximum extent of tsunami inundation in Newport, Oregon, for (a) present study with AEP = 0.0004, (b) ASCE Tsunami Design Geodatabase (TDG) for AEP = 0.0004, and (c) DOGAMI TIM, 'M' scenario (b and c are courtesy of ASCE TDG and Oregon Department of Geology and Mineral Industries).

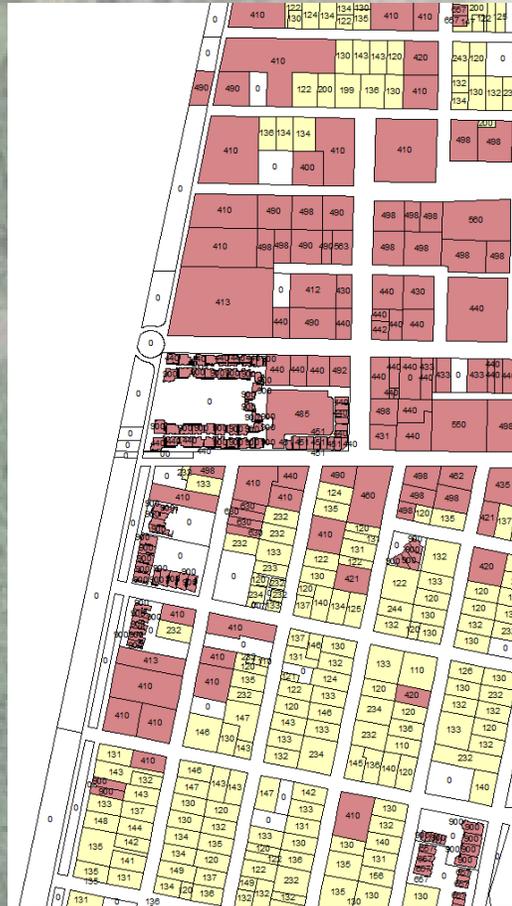


Three tools for building information at study area

1. Tax lot (Stat_Class, Year)

2. Pictures from Google map street view

3. Fields survey Rapid Visual Screening (RVS)



Rapid Visual Screening of Buildings for Potential Seismic Hazards
FEMA P-154 Data Collection Form

Level 1
VERY HIGH Seismicity

Address: 26 Ave H Zip: _____
 Other Identifiers: 06
 Building Name: Wordmark seaside
 Use: Hot. multiple buildings
 Latitude: 46.9929 Longitude: -123.9296
 S: _____ HP/Date/Time: 01/18/15, 11:45
 Screeners: _____
 No. Stories: Above Grade: 8 Below Grade: _____ Year Built: 2007 est
 Total Floor Area (sq. ft.): 532,264 Code Year: _____
 Additions: None Yes, Year(s) Built: _____
 Occupancy: Assembly Commercial Emer. Services Historic Shelter
 Industrial Office School Government
 Warehouse Residential # Units: _____

Soil Type: A Hard Rock C Avg. Dense Soil D Soft Soil E Floor DNK assume Type D.

Geologic Hazards: Liquefaction: Yes/No/DNK Landslide: Yes/No/DNK Surf. Rupt. Yes/No/DNK
 Adjacency: Founding Falling Hazards from Taller Adjacent Building
 Irregularities: Vertical (topsoverly) Plan (type) reentrant corner
 Exterior Falling Hazards: Unbraced Chimneys Heavy Chalking or Heavy Veneer
 Parapets Appendages
 Other: Glasses

COMMENTS:
288 condors
1600'
parking: PC2
 -Multiple adjacent building.
 -Construction joint not visible
 -Ground floor is used for commercial purpose.

SKETCH Dimensions added from Google earth - H.P. = _____
 Additional sketches or comments on separate page

| FEMA BUILDING TYPE | Do Not Know | W1 | W1A | W2 | S1 (W1) | S2 (W1) | S3 (W1) | S4 (W1) | S5 (W1) | C1 (W1) | C2 (W1) | C3 (W1) | PC1 (W1) | PC2 (W1) | PC3 (W1) | PC4 (W1) | URM | MH |
|--|-------------|-----|-----|-----|---------|---------|---------|---------|---------|---------|---------|---------|----------|----------|----------|----------|-----|-----|
| Basic Score | 2.1 | 1.9 | 1.8 | 1.5 | 1.4 | 1.6 | 1.4 | 1.2 | 1.6 | 1.2 | 0.9 | 1.1 | 1.0 | 1.1 | 1.1 | 1.1 | 0.9 | 1.1 |
| Severe Vertical Irregularity, V _v | 0.9 | 0.9 | 0.9 | 0.7 | 0.8 | 0.7 | 0.7 | 0.7 | 0.7 | 0.8 | 0.6 | 0.7 | 0.7 | 0.7 | 0.7 | 0.7 | 0.6 | NA |
| Moderate Vertical Irregularity, V _m | 0.6 | 0.5 | 0.5 | 0.4 | 0.4 | 0.5 | 0.4 | 0.3 | 0.4 | 0.4 | 0.3 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 | 0.3 | NA |
| Plus Irregularity, P ₁ | 0.7 | 0.7 | 0.6 | 0.5 | 0.5 | 0.6 | 0.4 | 0.4 | 0.4 | 0.5 | 0.3 | 0.5 | 0.4 | 0.4 | 0.4 | 0.4 | 0.3 | NA |
| Pre-Code | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.2 | 0.1 | 0.1 | 0.2 | 0.0 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.0 | 0.0 |
| Post-Benchmark | 1.9 | 1.8 | 2.0 | 1.7 | 1.1 | 1.1 | 1.5 | NA | 1.4 | 1.7 | NA | 1.5 | 1.7 | 1.6 | 1.6 | 1.6 | NA | 2.0 |
| Soil Type A or B | 0.5 | 0.5 | 0.4 | 0.3 | 0.3 | 0.4 | 0.3 | 0.2 | 0.3 | 0.3 | 0.1 | 0.3 | 0.2 | 0.3 | 0.3 | 0.3 | 0.1 | 0.1 |
| Soil Type E (1-3 stories) | 0.0 | 0.2 | 0.4 | 0.3 | 0.2 | 0.2 | 0.2 | 0.1 | 0.1 | 0.2 | 0.0 | 0.2 | 0.1 | 0.2 | 0.1 | 0.2 | 0.0 | 0.1 |
| Soil Type E (> 3 stories) | 0.4 | 0.4 | 0.4 | 0.3 | 0.3 | NA | 0.3 | 0.1 | 0.1 | 0.3 | 0.1 | NA | 0.1 | 0.2 | 0.2 | 0.0 | NA | NA |
| Minimum Score, S _{min} | 0.7 | 0.7 | 0.7 | 0.5 | 0.5 | 0.5 | 0.5 | 0.3 | 0.3 | 0.3 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 |

FINAL LEVEL 1 SCORE, S_{L1} & S_{min}: **2.0** **2.0** Use, 2.0

EXTENT OF REVIEW
 Exterior: Partial All Sides Awful
 Interior: None Visible Entered
 Drawing Reviewed: Yes No
 Soil Type Source: _____
 Geologic Hazards Source: _____
 Contact Person: _____

OTHER HAZARDS
 Are There Hazards That Trigger A Detailed Structural Evaluation?
 Yes, unknown FEMA building type or other building
 Yes, score less than cut-off
 Yes, other hazards present
 No
 Founding hazards from taller adjacent building
 Falling hazards from taller adjacent building
 Geologic hazards or Soil Type F
 Significant damage/deterioration to the structural system

ACTION REQUIRED
 Detailed Structural Evaluation Required?
 Yes, unknown FEMA building type or other building
 Yes, score less than cut-off
 Yes, other hazards present
 No
 Detailed Nonstructural Evaluation Recommended? (check one)
 Yes, nonstructural hazards identified that should be evaluated
 No, nonstructural hazards exist that may require mitigation, but a detailed evaluation is not necessary
 No, no nonstructural hazards identified DNK

LEVEL 2 SCREENING PERFORMED?
 Nonstructural hazards? Yes No

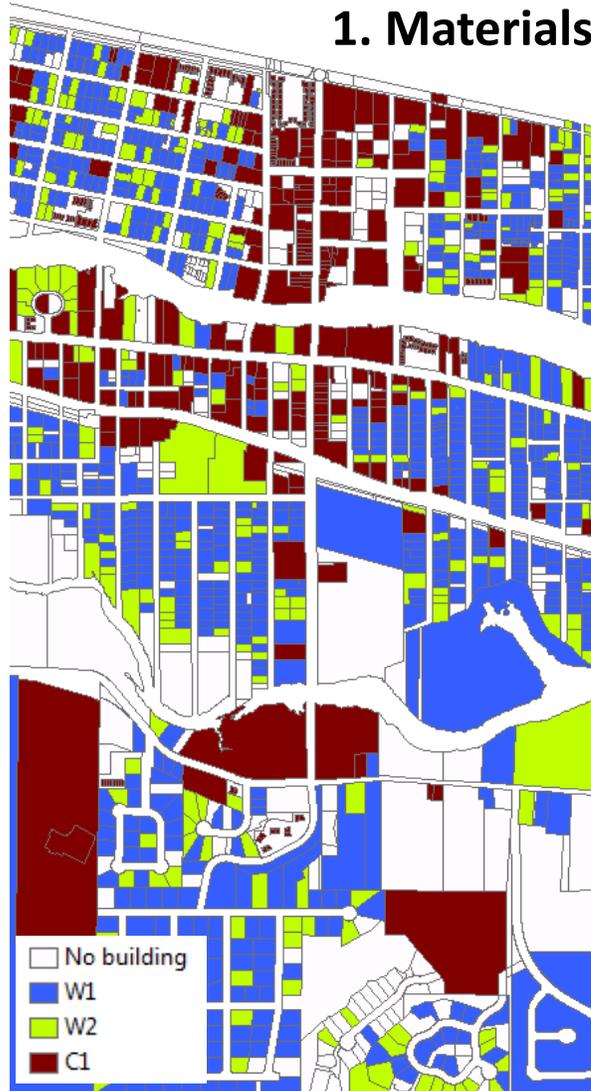
Where information cannot be verified, screener shall note the following: EST = Estimated or unreliable data DNK = Do Not Know

Legend
 BR = Braced frame RC = Reinforced concrete SW = Shear wall TU = Tilt up
 MR = Moment-resisting frame UNK = Unreliable necessary info LM = Light metal PC = Rigid diaphragm



Building Classification

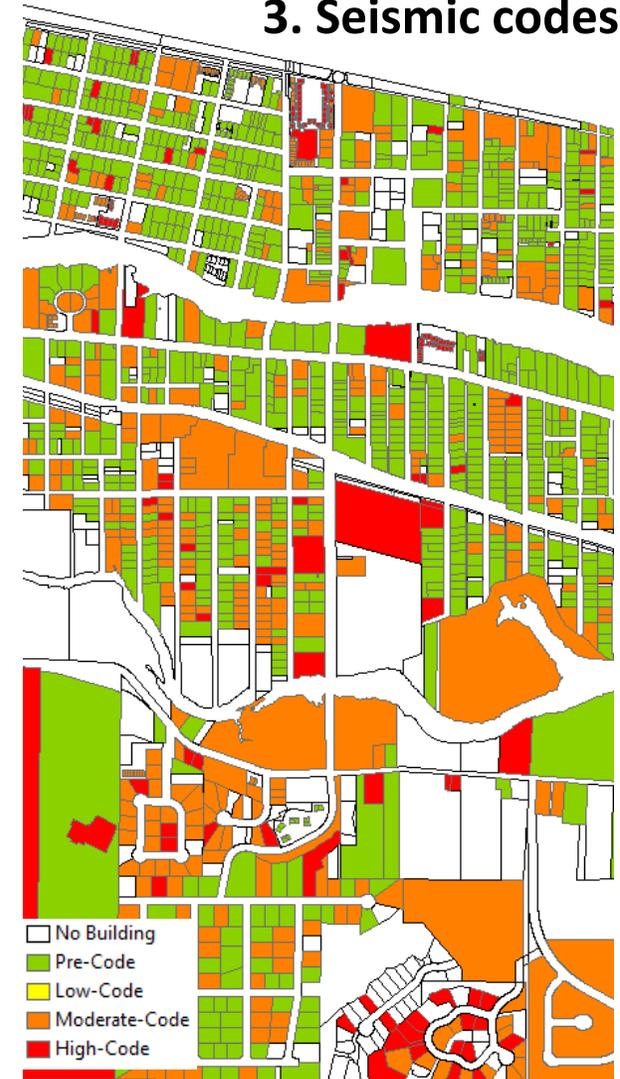
1. Materials



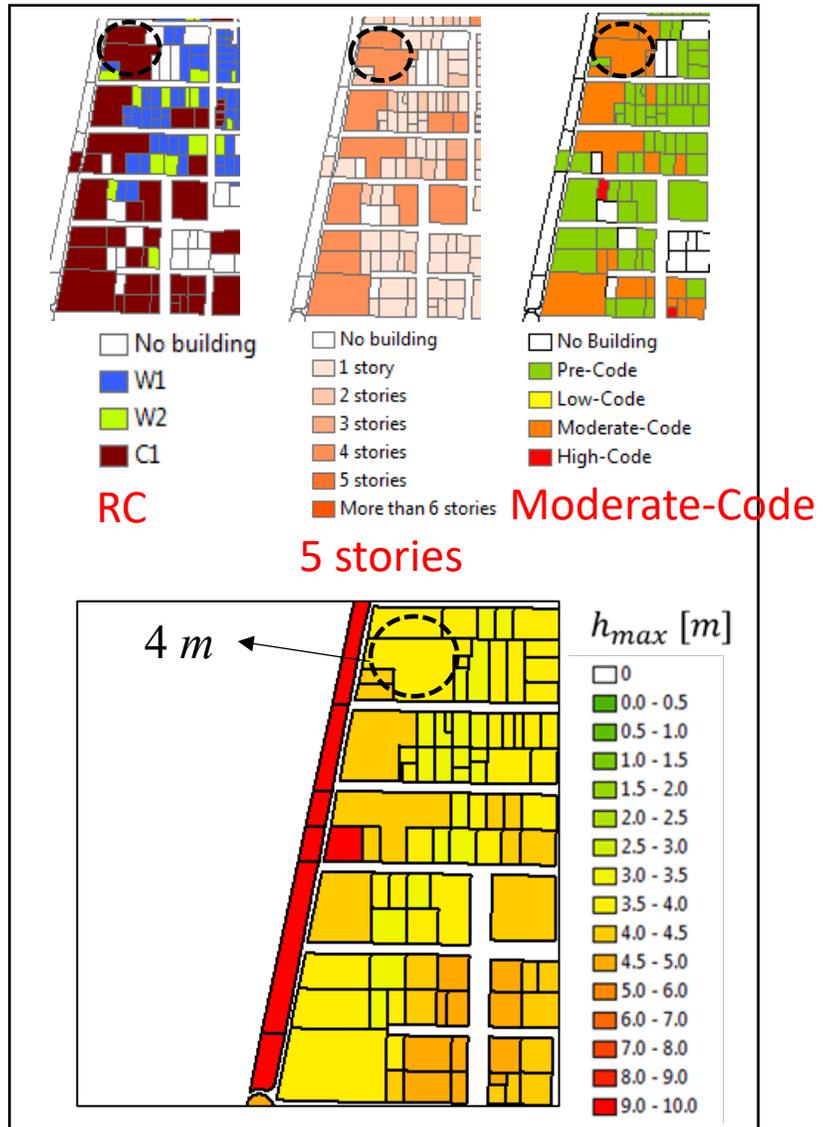
2. Floors



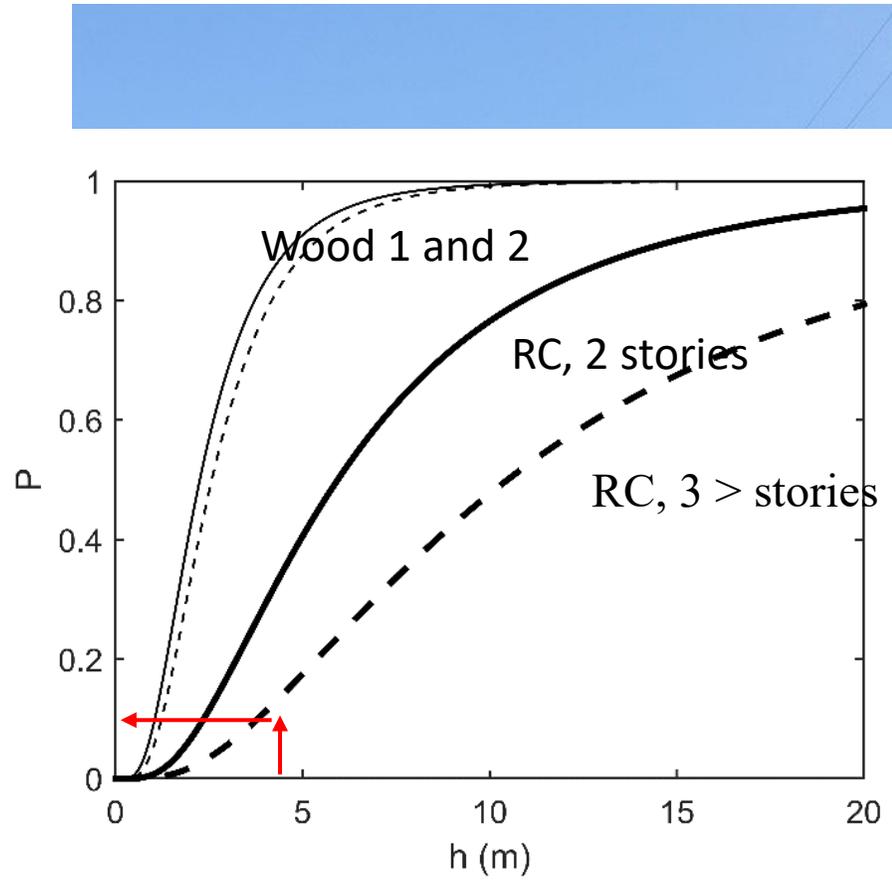
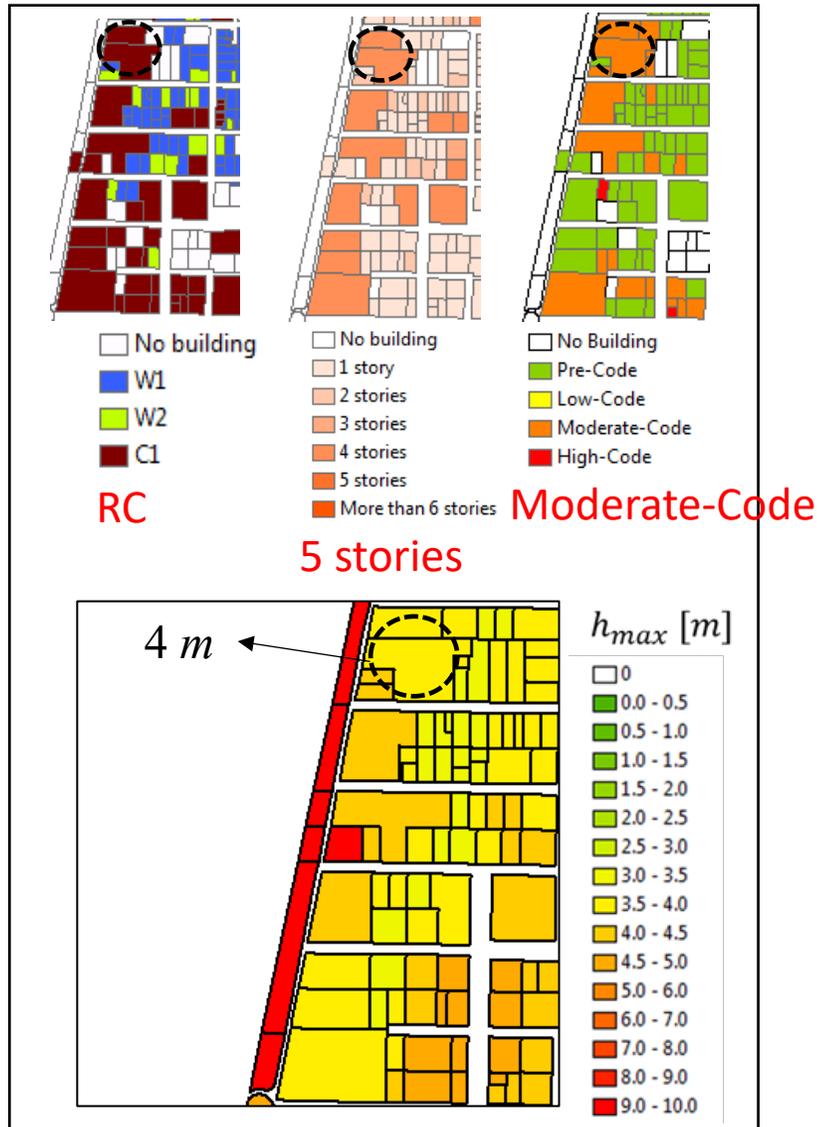
3. Seismic codes



Example of building damage assessment (at AEP = 0.001)

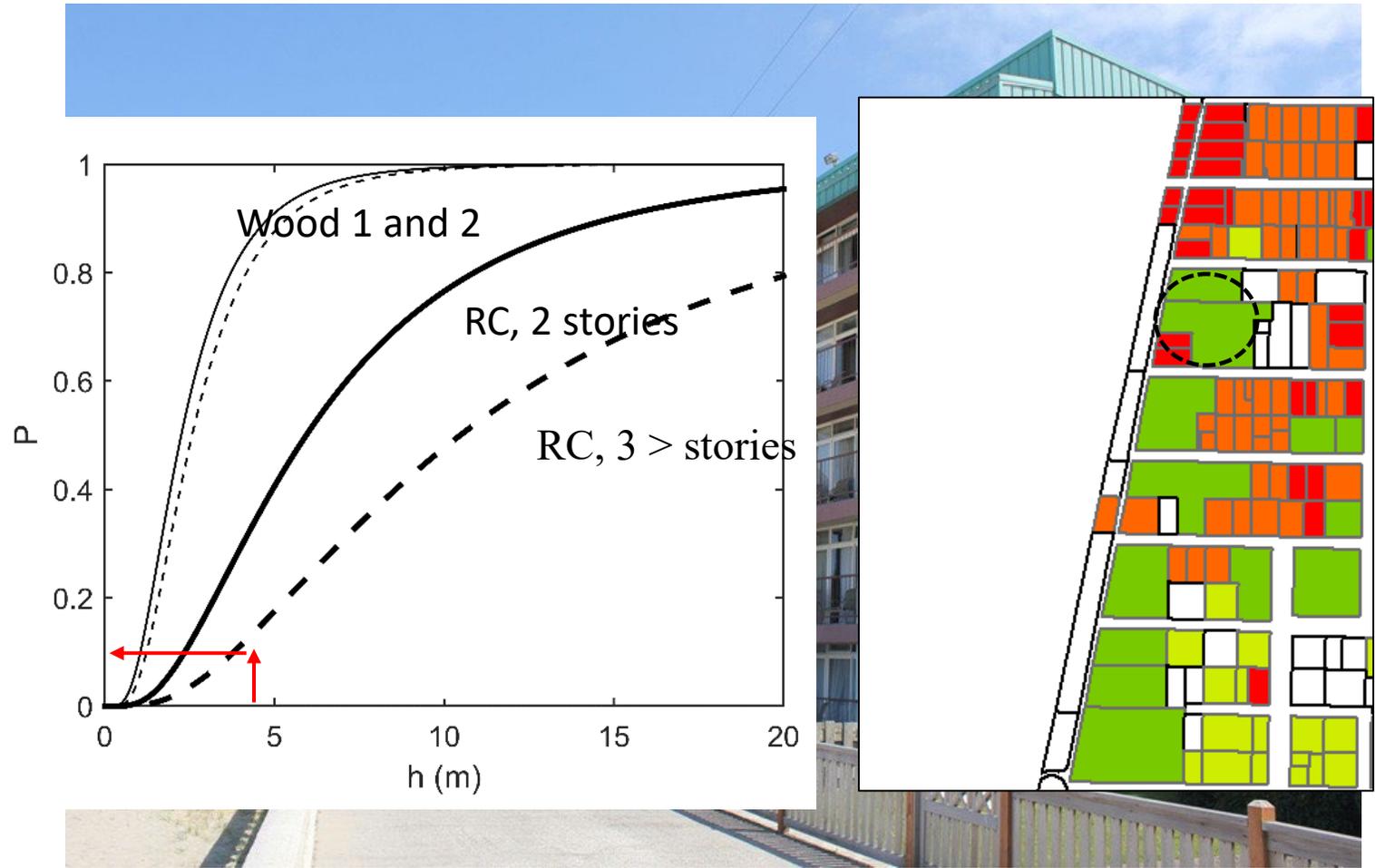
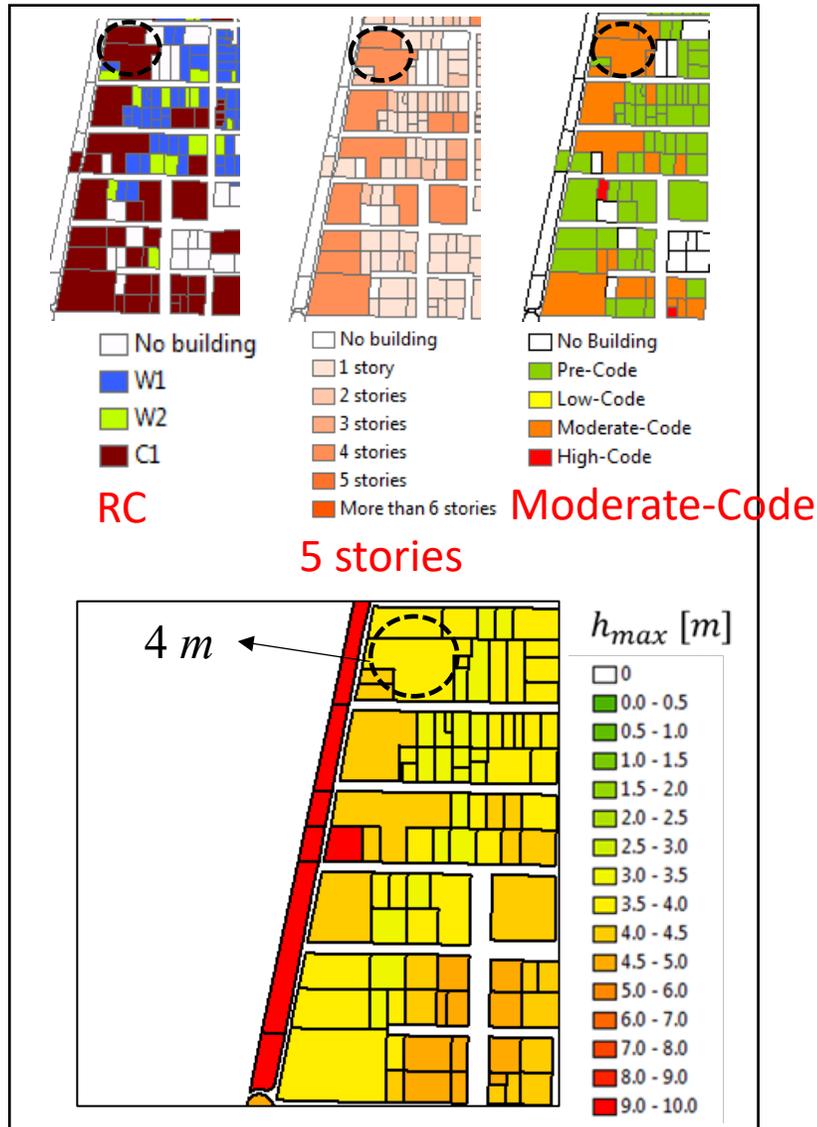


Example of building damage assessment (at AEP = 0.001)



Fragility curves (Suppasri et al., 2013) for collapse damage

Example of building damage assessment (at AEP = 0.001)



Fragility curves (Suppasri et al., 2013) for collapse damage

Example of building damage assessment (at AEP = 0.001)

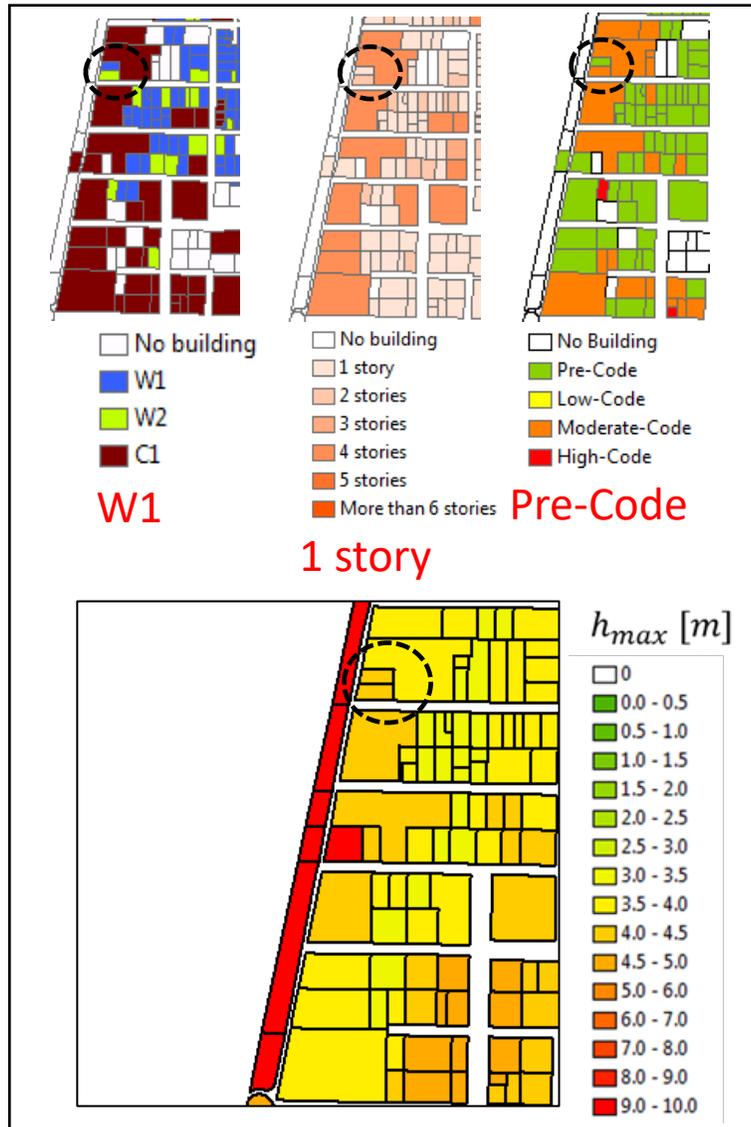
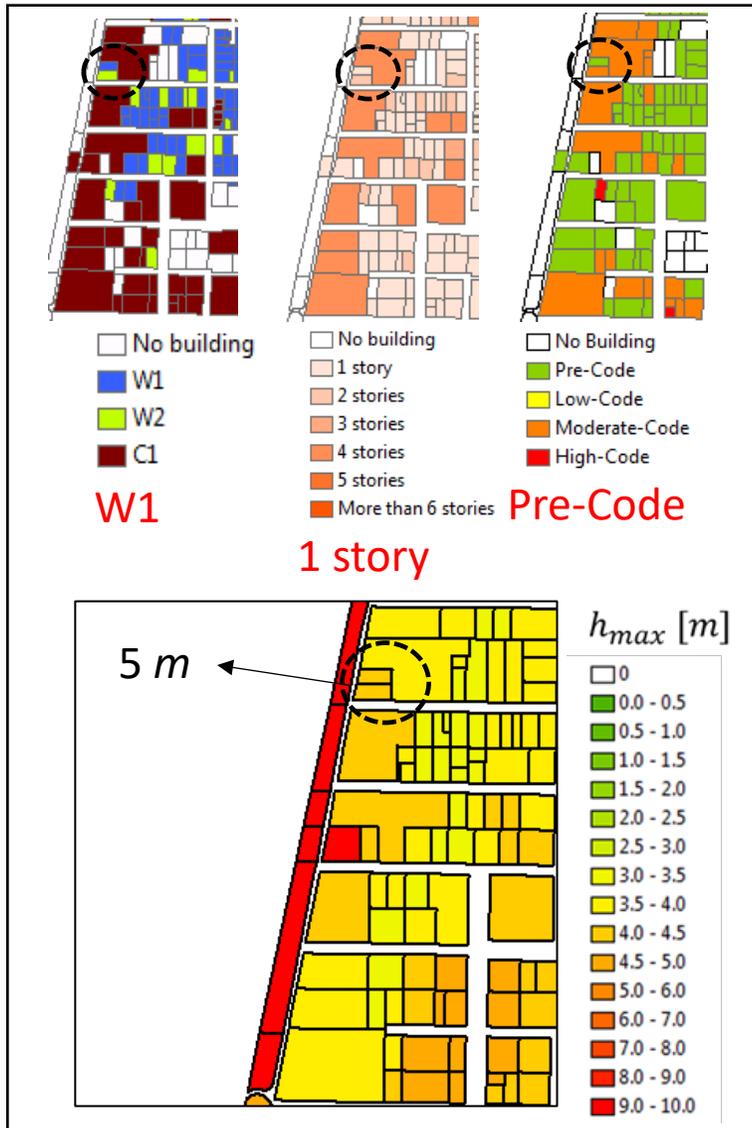
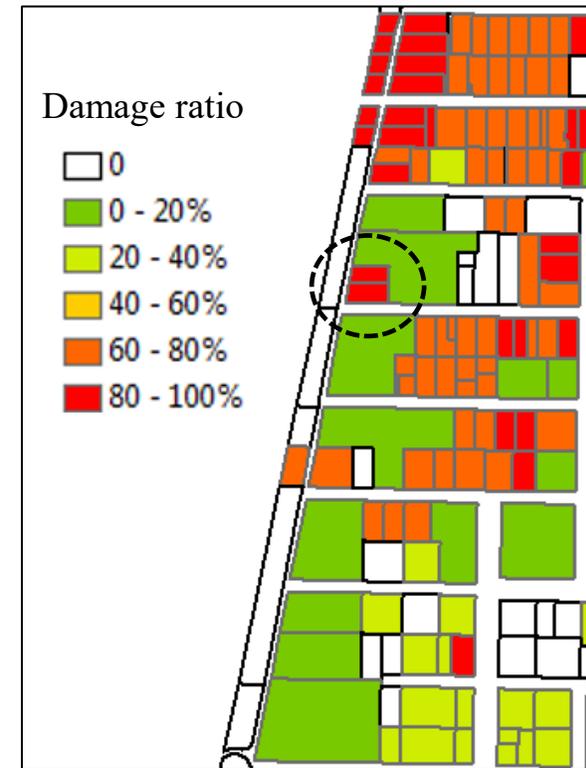
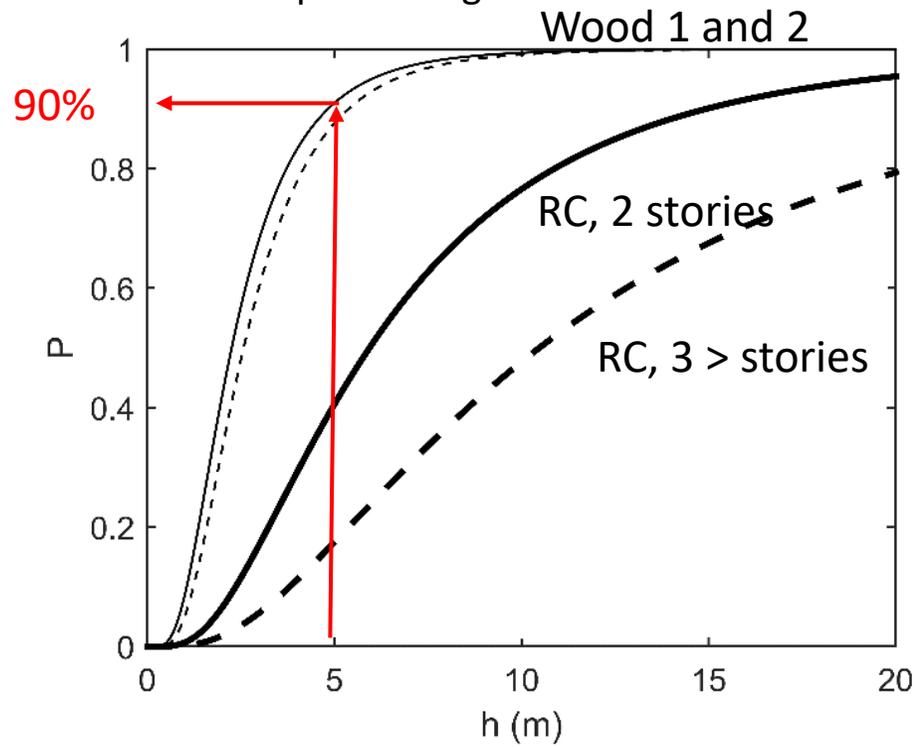


Photo taken by Hyongsu Park, at Seaside Field trip (July, 14, 2015)

Example of building damage assessment (at AEP = 0.001)



Fragility curves (Suppasri et al., 2013) for Collapse damage



Probability damage at AEP = 0.001 (~1,000 year event)
at CSZ with S2013 model (h_{max} , Collapse DS)



Earthquake Only

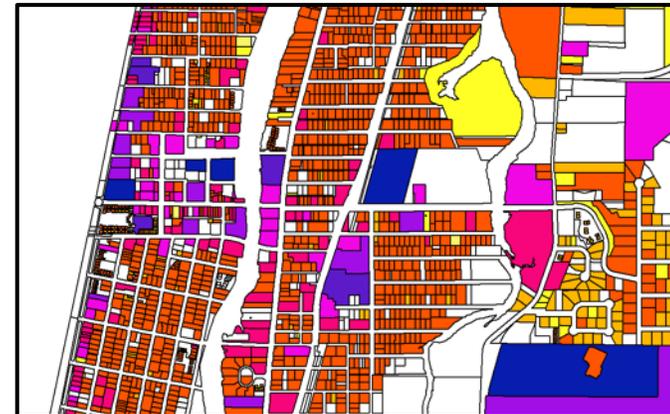
Tsunami Only

Combined

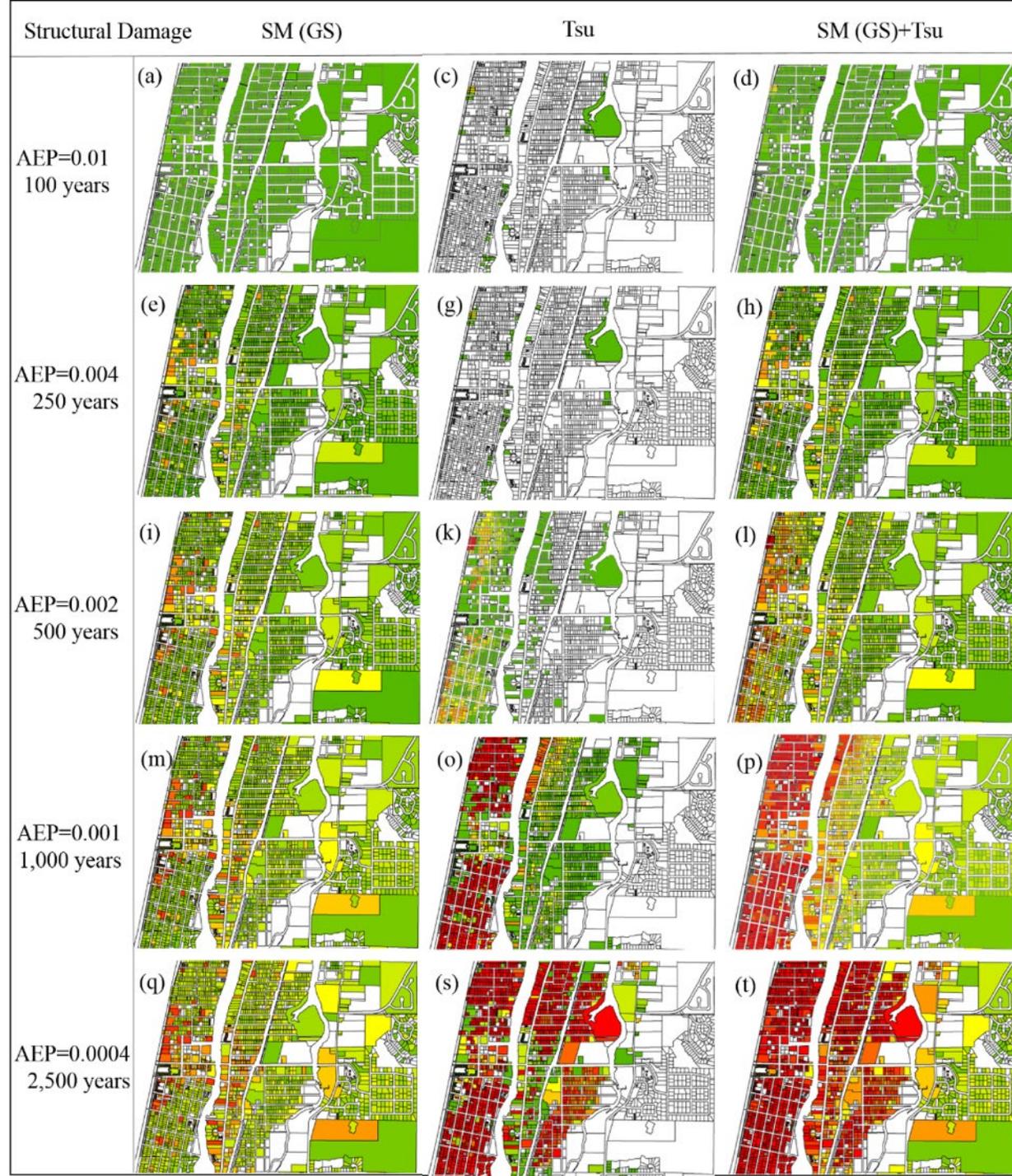
AEP=0.001
1,000 years

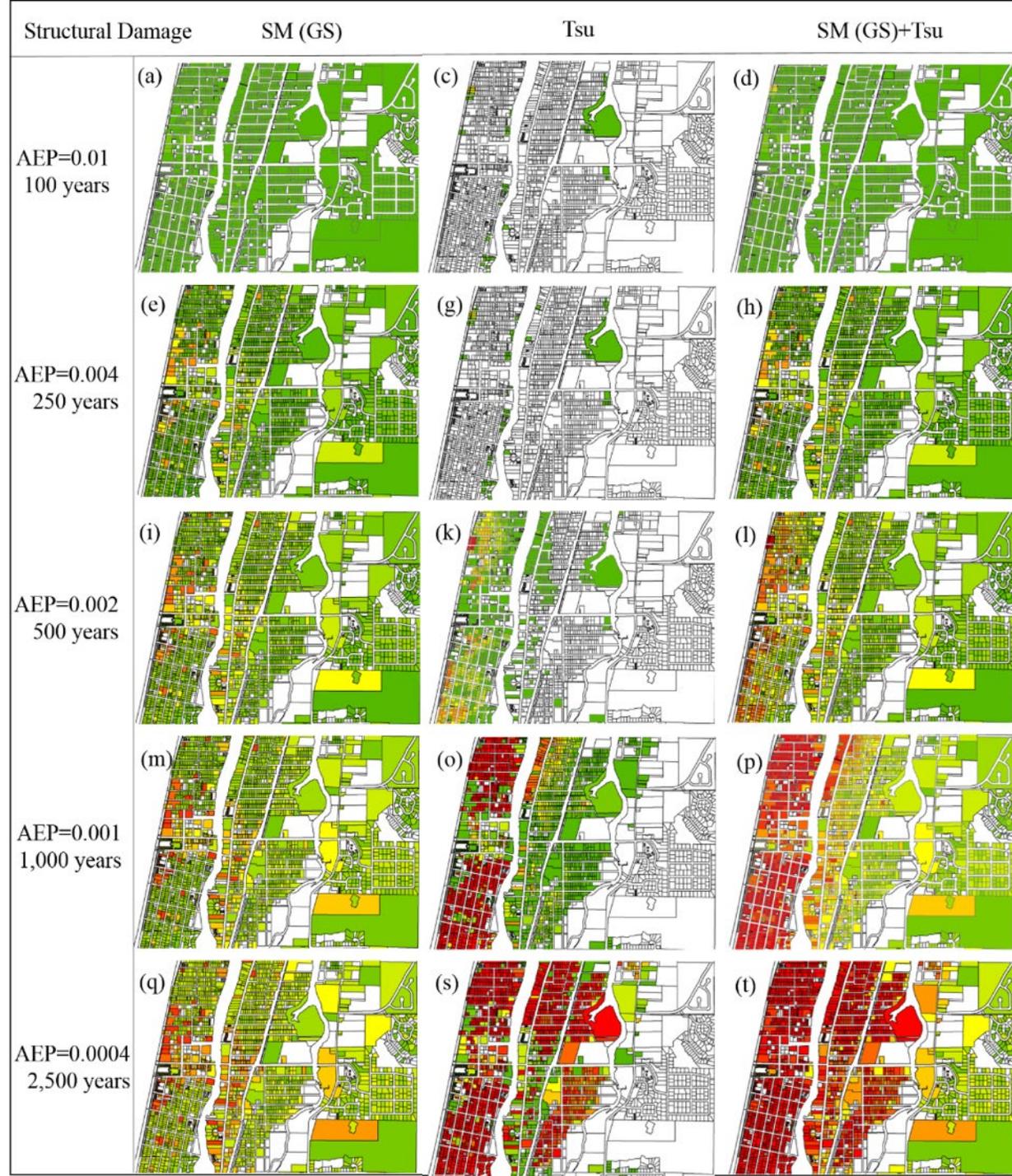


Park, H, MS Alam, DT Cox, AR Barbosa, JW van de Lindt (2019) "Probabilistic seismic and tsunami damage analysis (PSTDA) for the Cascadia Subduction Zone applied to Seaside, Oregon," *International Journal of Disaster Risk Reduction*, 35, 101076, <https://doi.org/10.1016/j.ijdr.2019.101076>.



TSU + EQ
Loss total: 1,230 M





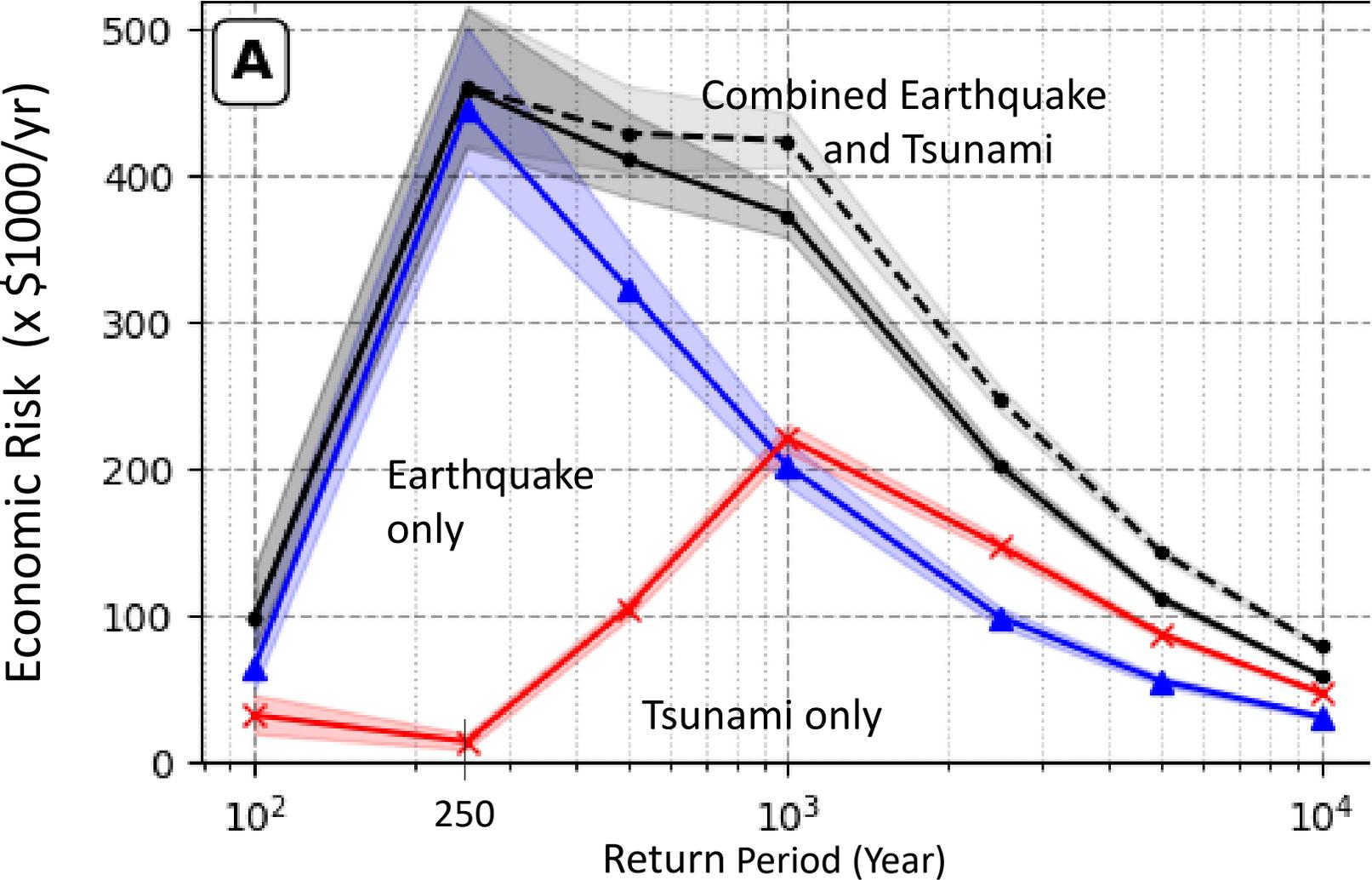
Higher probability
Lower consequences



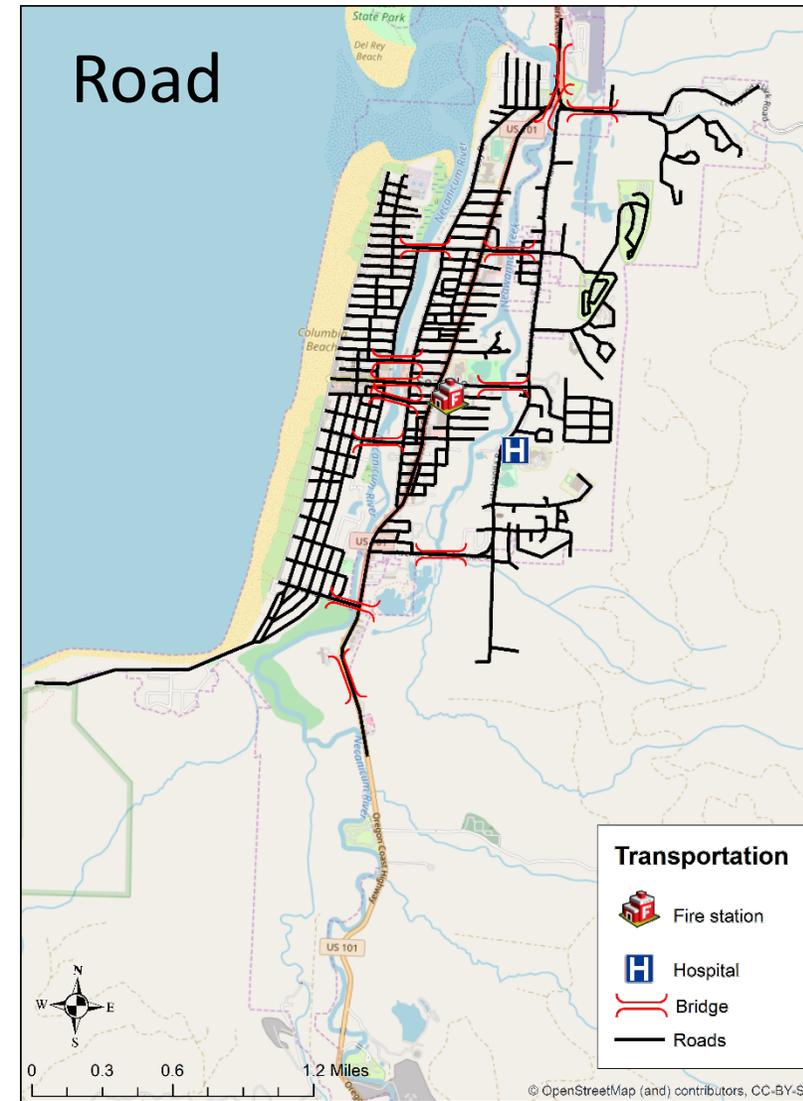
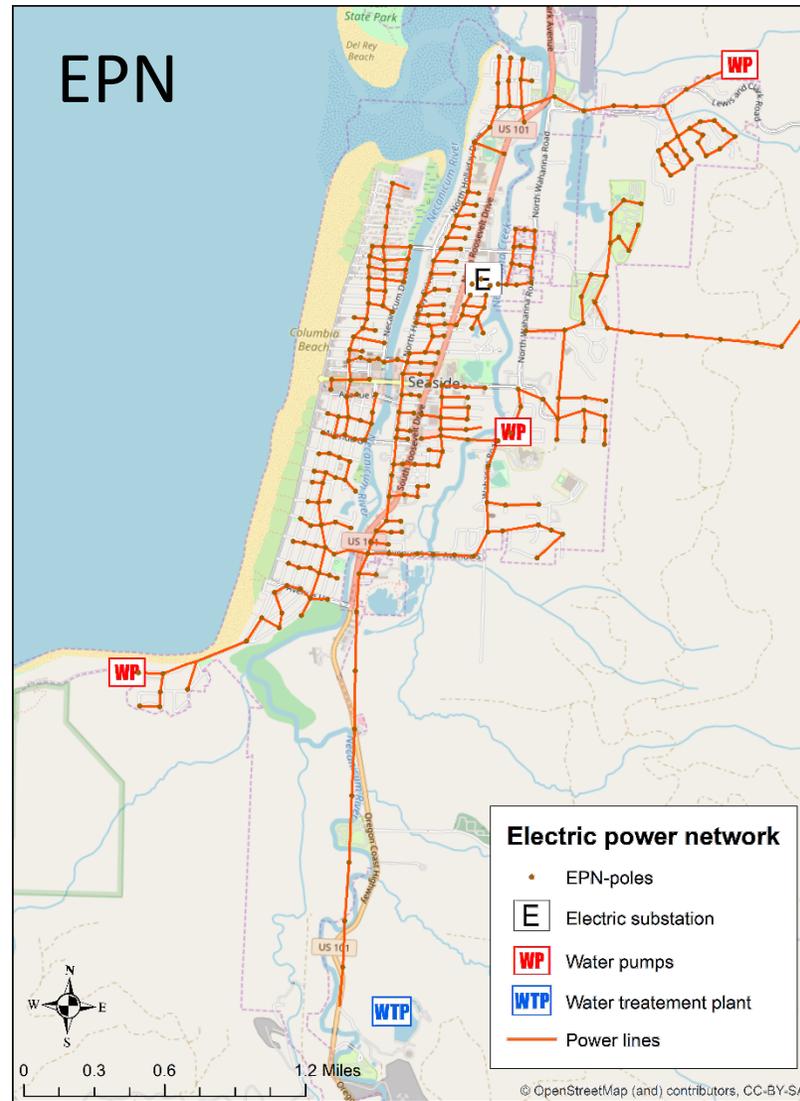
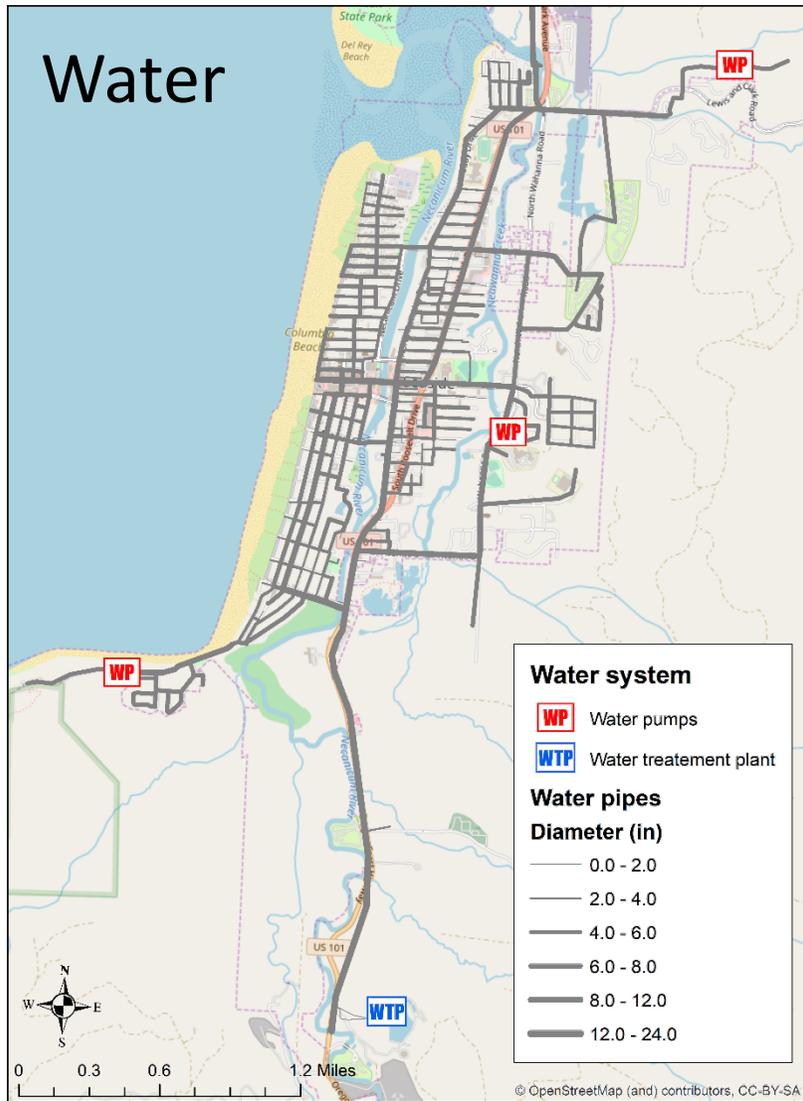
Highest
Risk

Lower probability
Higher consequences

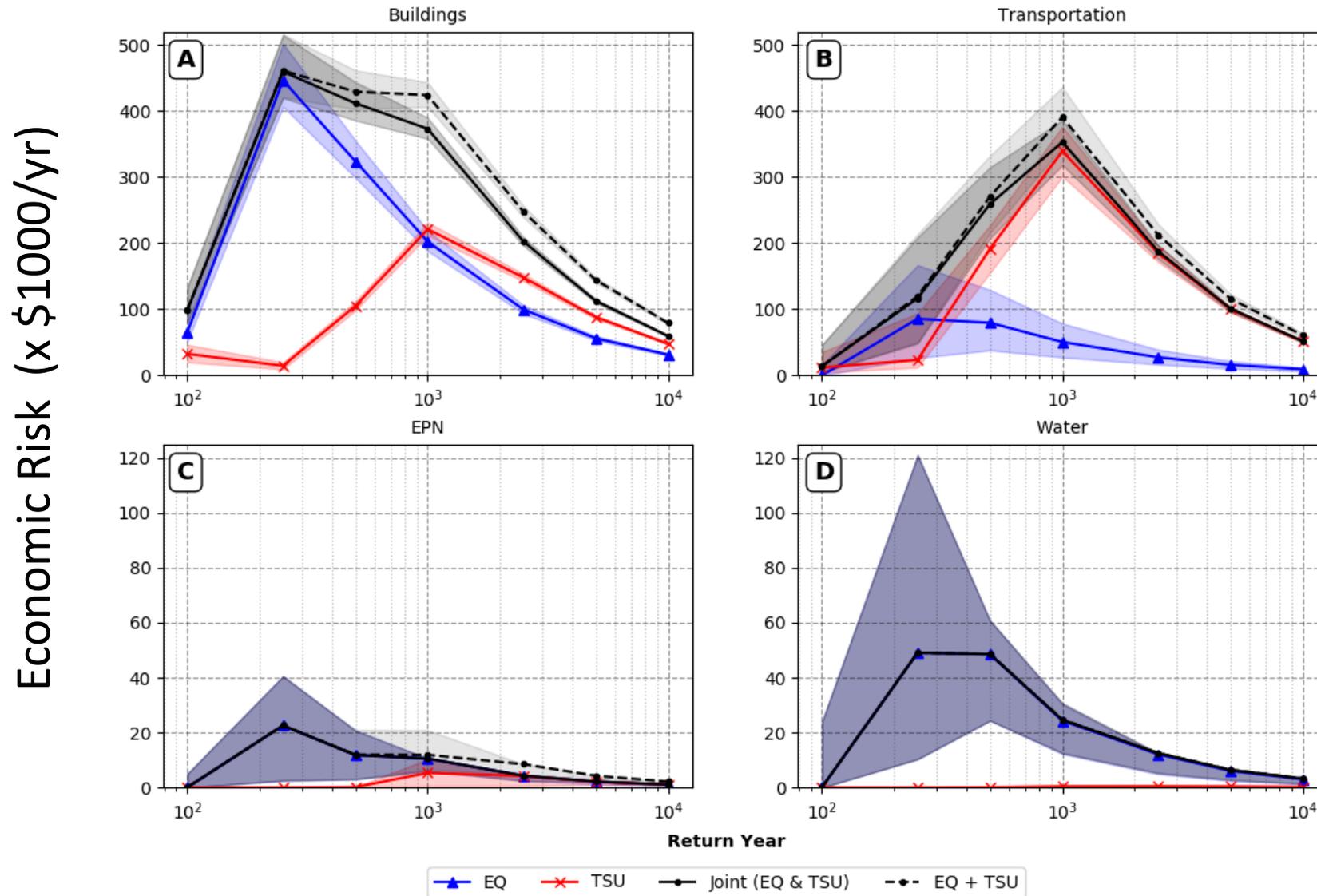
Annualized Risk for Building Damages in Seaside



Critical (lifeline) infrastructure networks

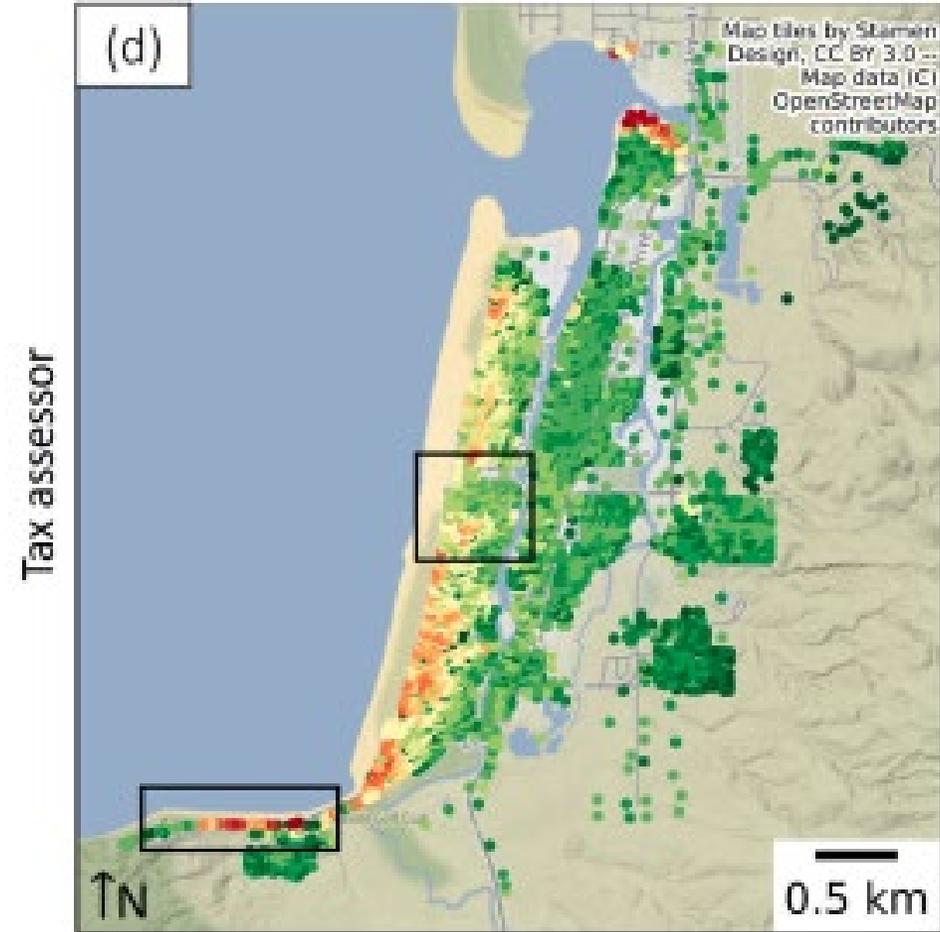
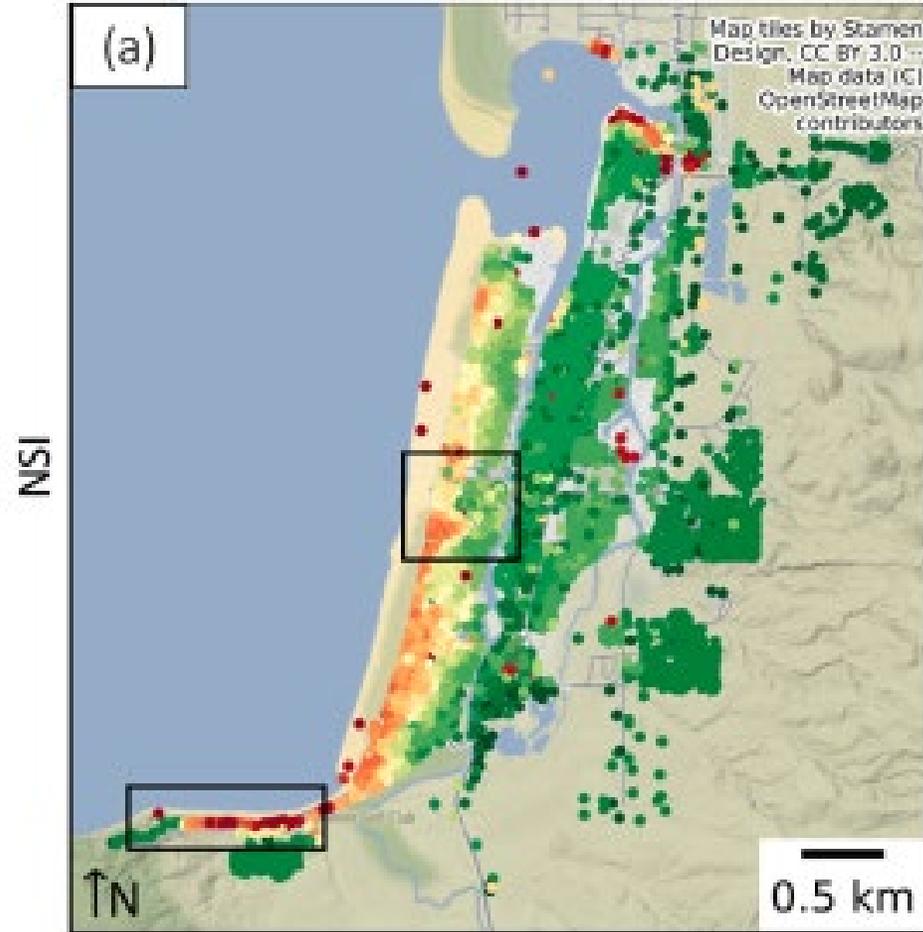


Annualized Risk for Building Damages in Seaside



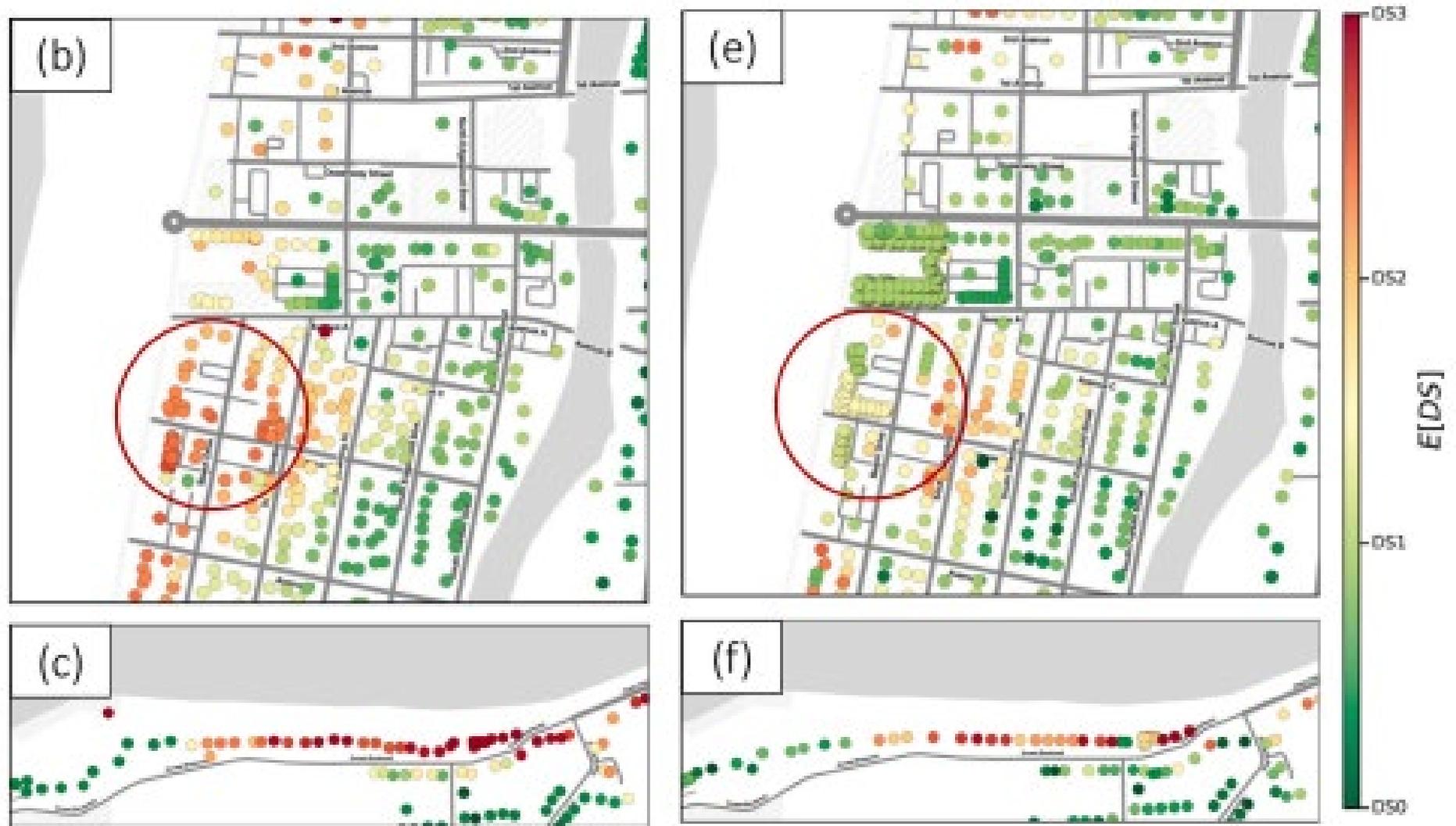
Sanderson D, S Kameshwar, N Rosenheim, DT Cox (2021) "Deaggregation of multi-hazard damages, losses, risks, and connectivity: An application to the joint seismic-tsunami hazard at Seaside, Oregon," *Natural Hazards*, <https://doi.org/10.1007/s11069-021-04900-9>.

Uncertainty in the building stock



Sanderson D, DT Cox (2023) "Comparison of national and local building inventories for damage and loss modeling of seismic and tsunami hazards: From parcel-to-city-scale" *International Journal of Disaster Risk Reduction*, <https://doi.org/10.1016/j.ijdrr.2023.103755>

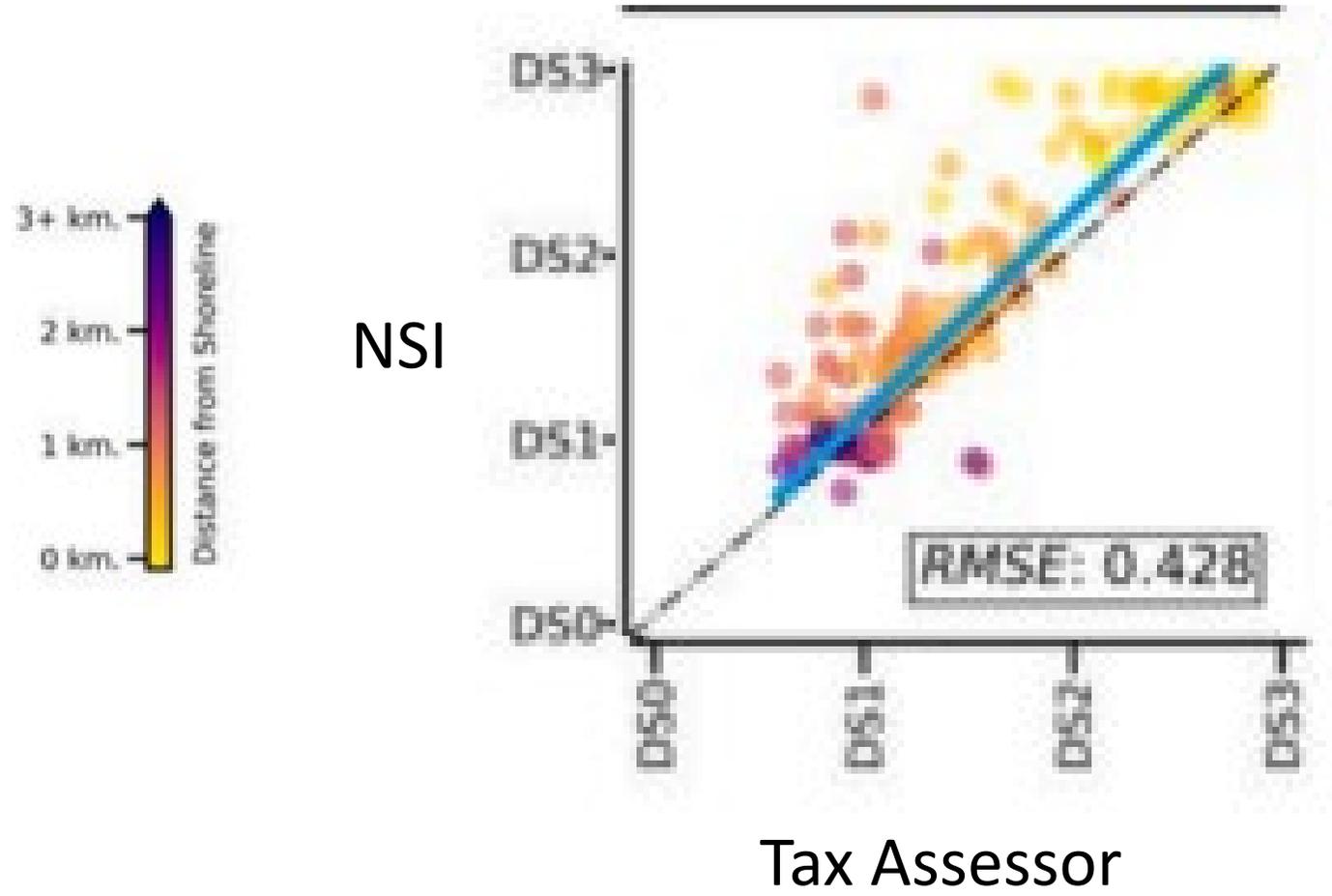
Uncertainty in the building stock



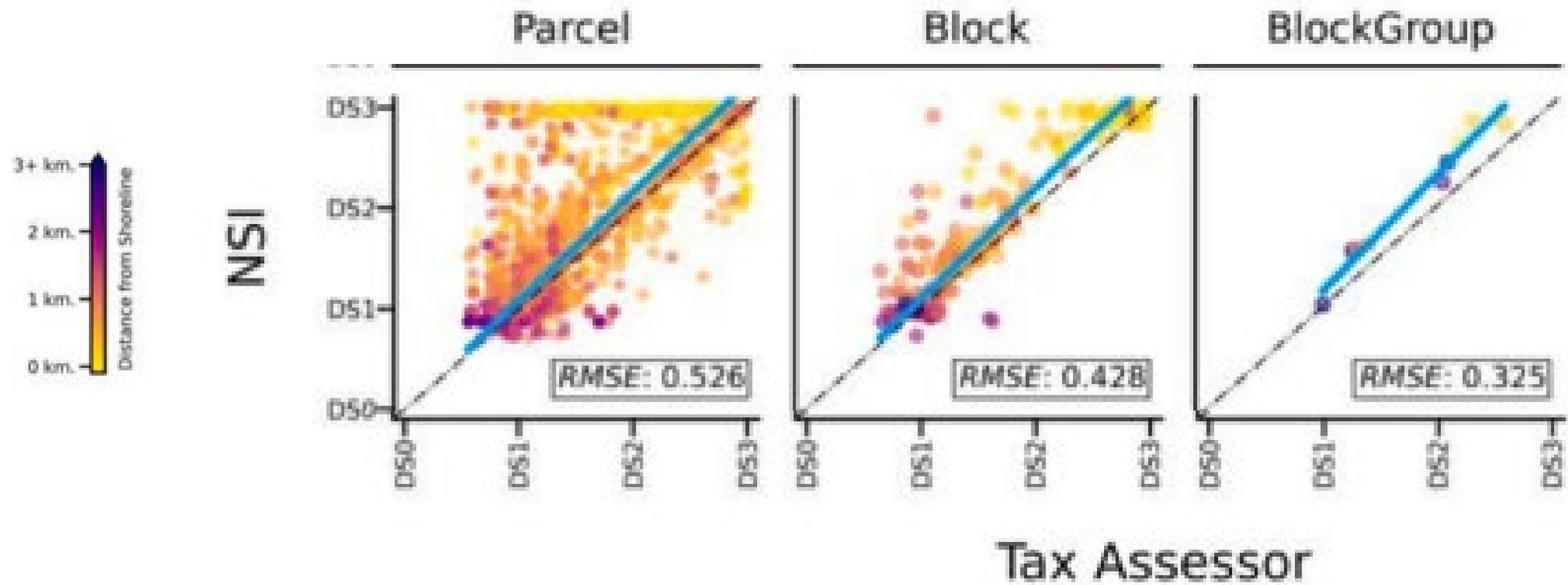
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Uncertainty in the building stock

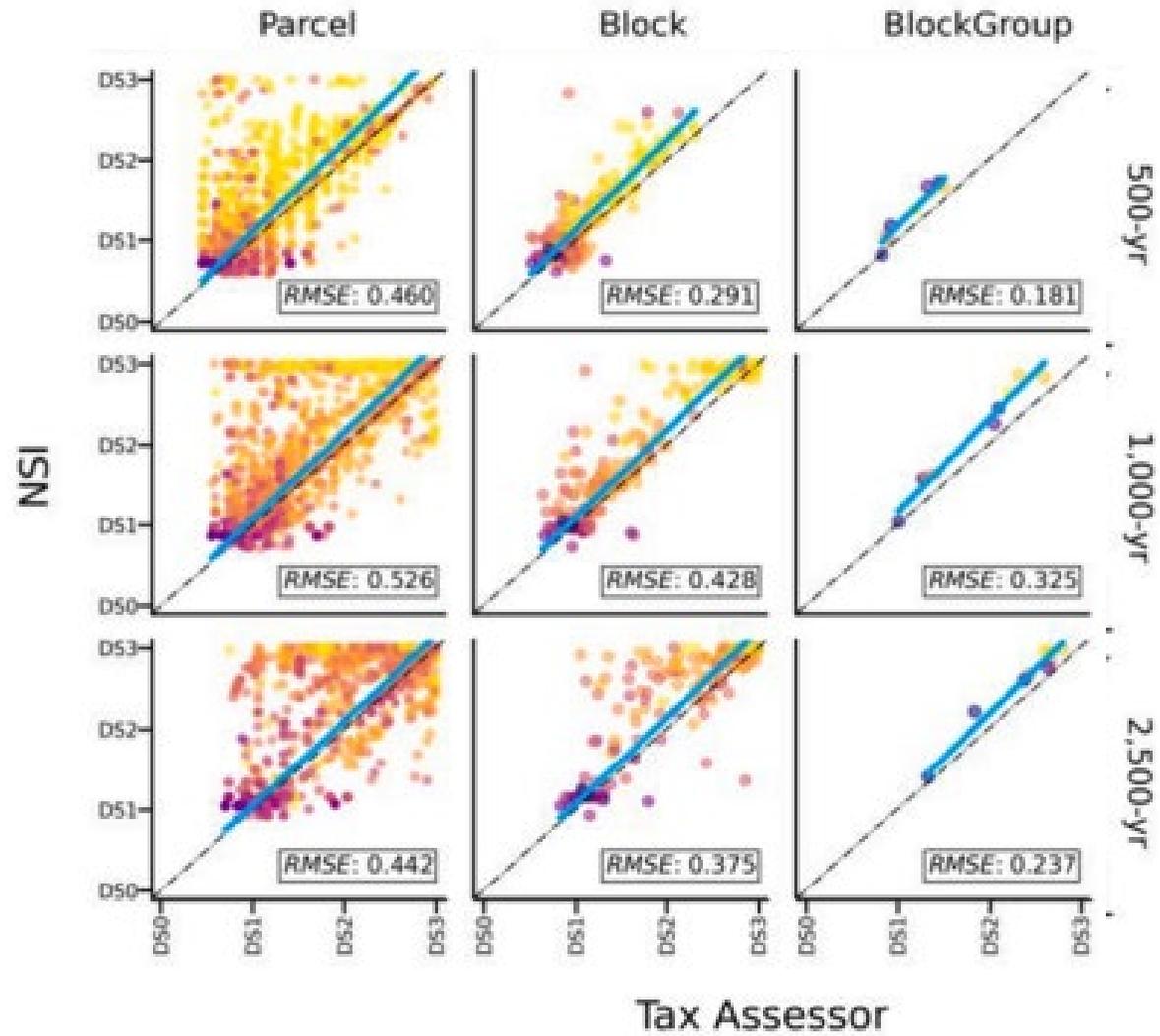
1,000 yr event Block Level



Uncertainty in the building stock

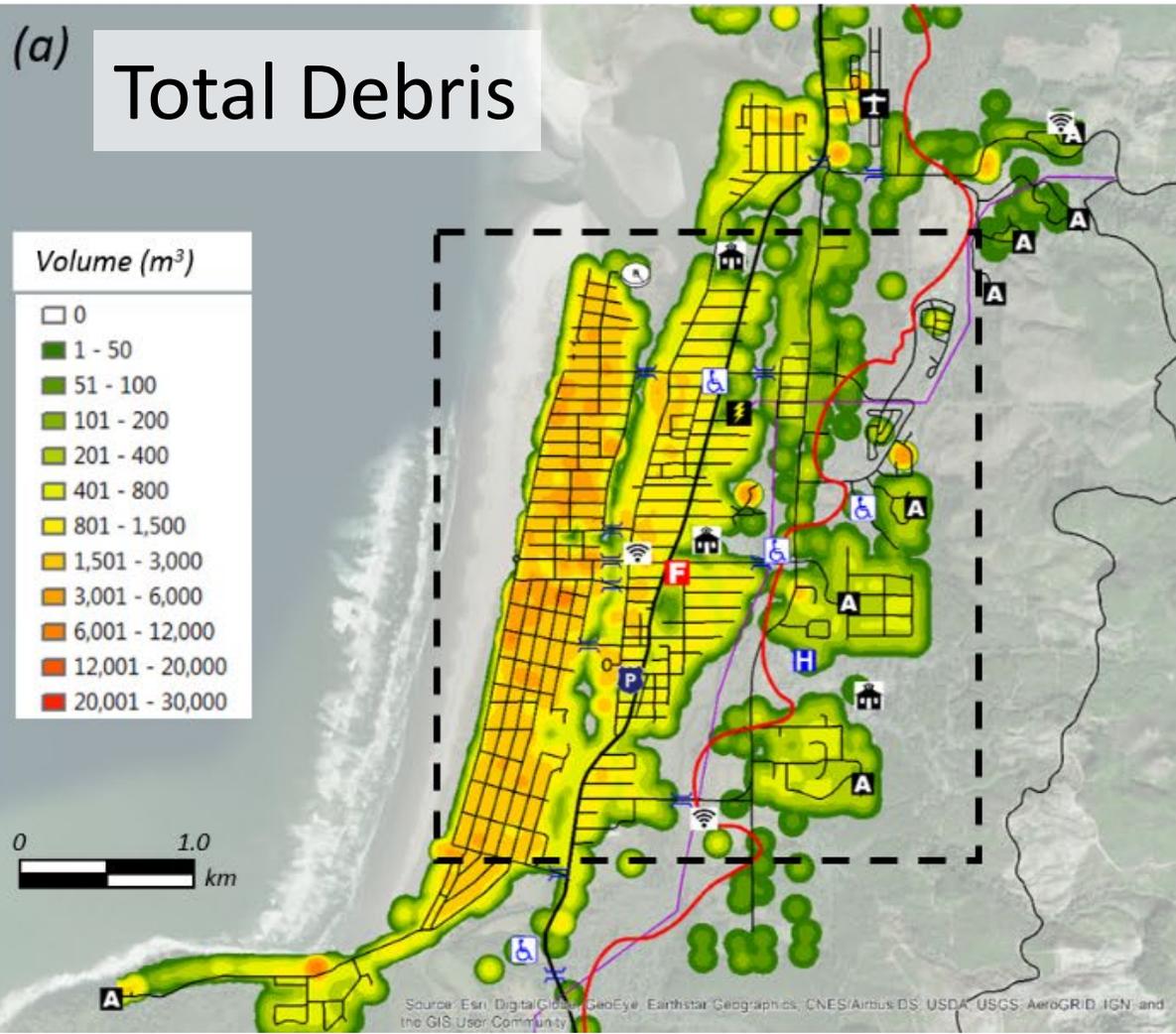
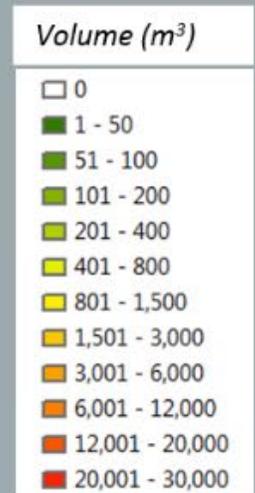


Uncertainty in the building stock

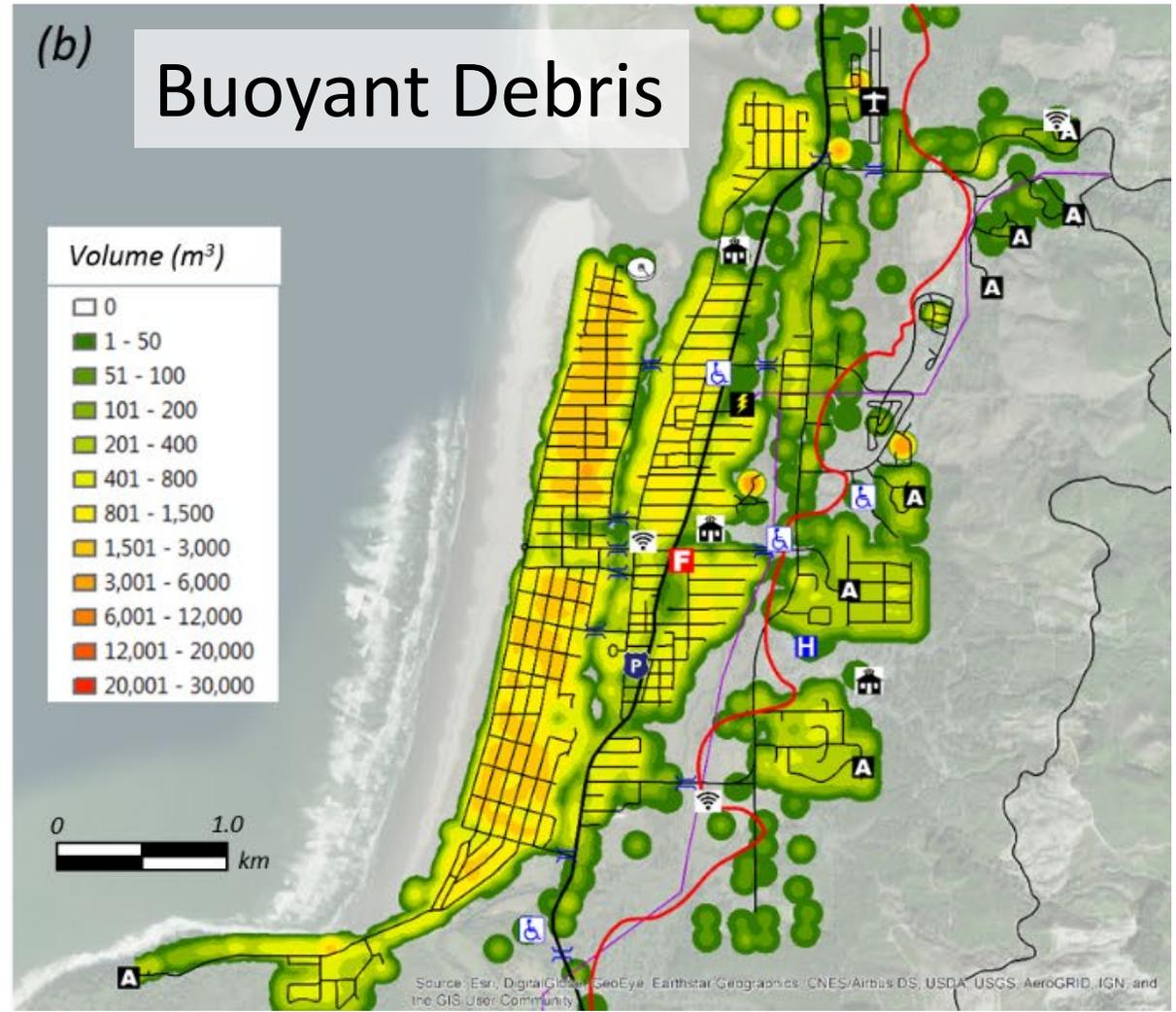
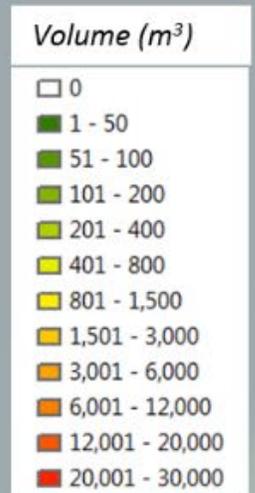




(a) Total Debris

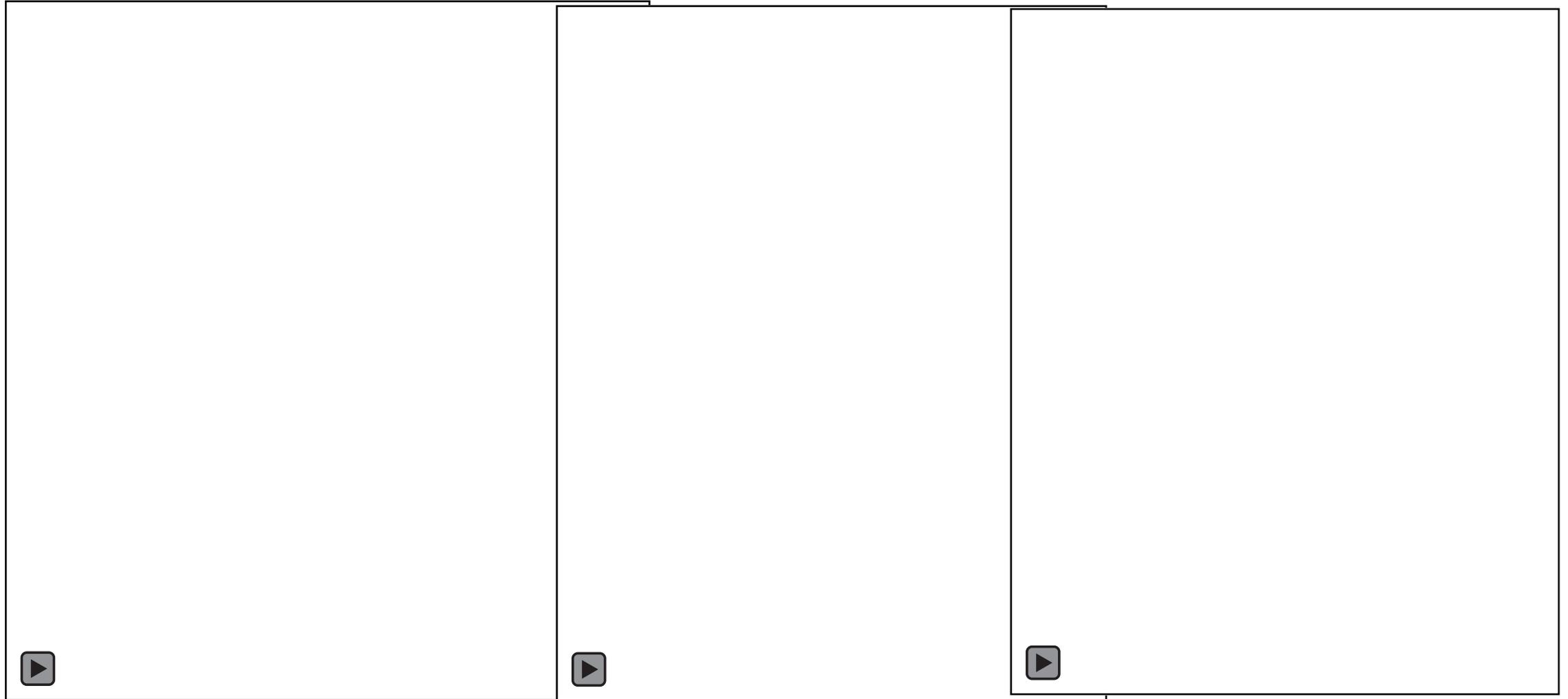


(b) Buoyant Debris



Distribution of expected debris volume (m³) per unit area (hectare) for 1000 year event without advection. (a) Volume of total debris from EQ+TSU, (b) Volume of buoyant debris only from EQ+TSU.

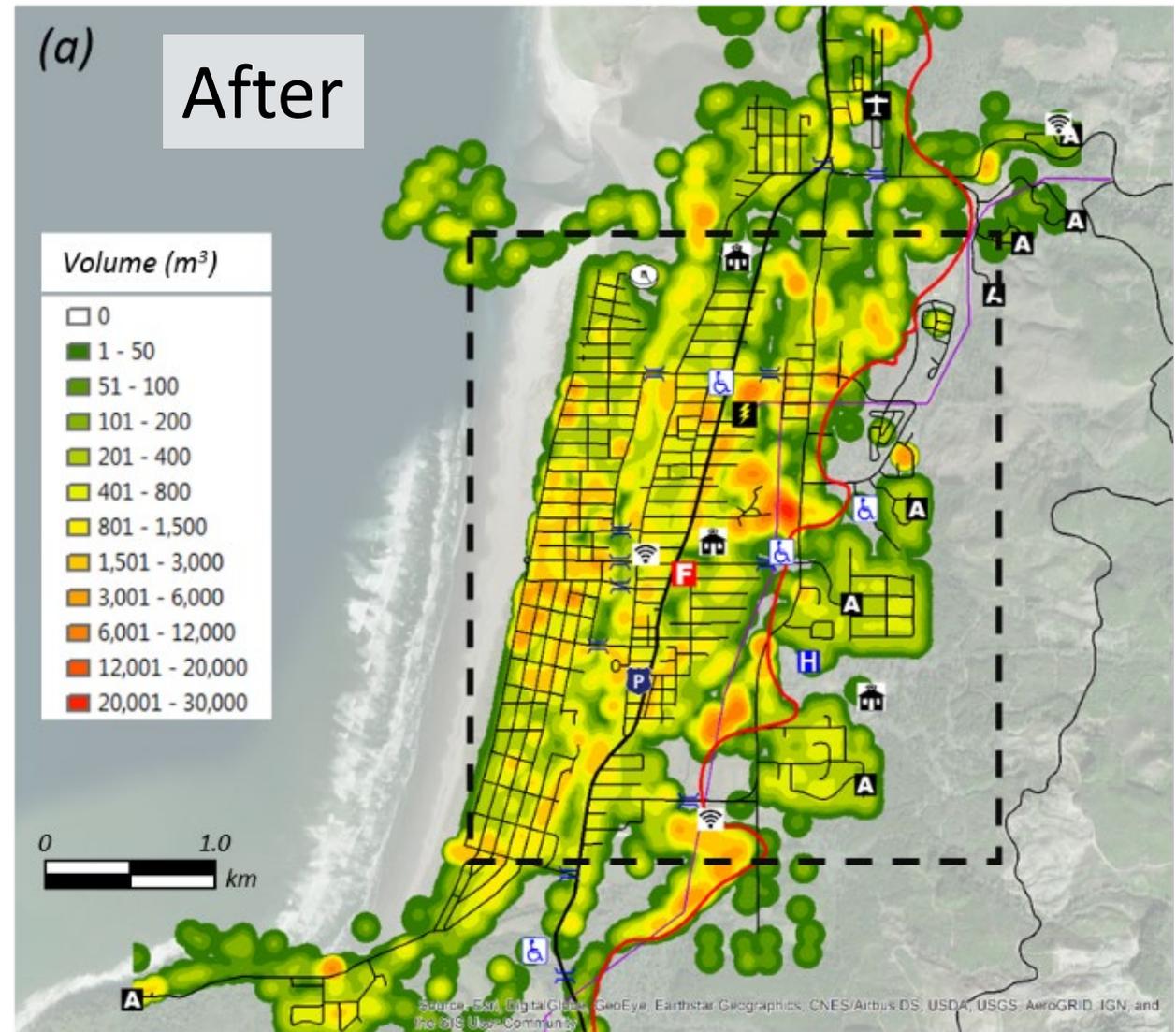
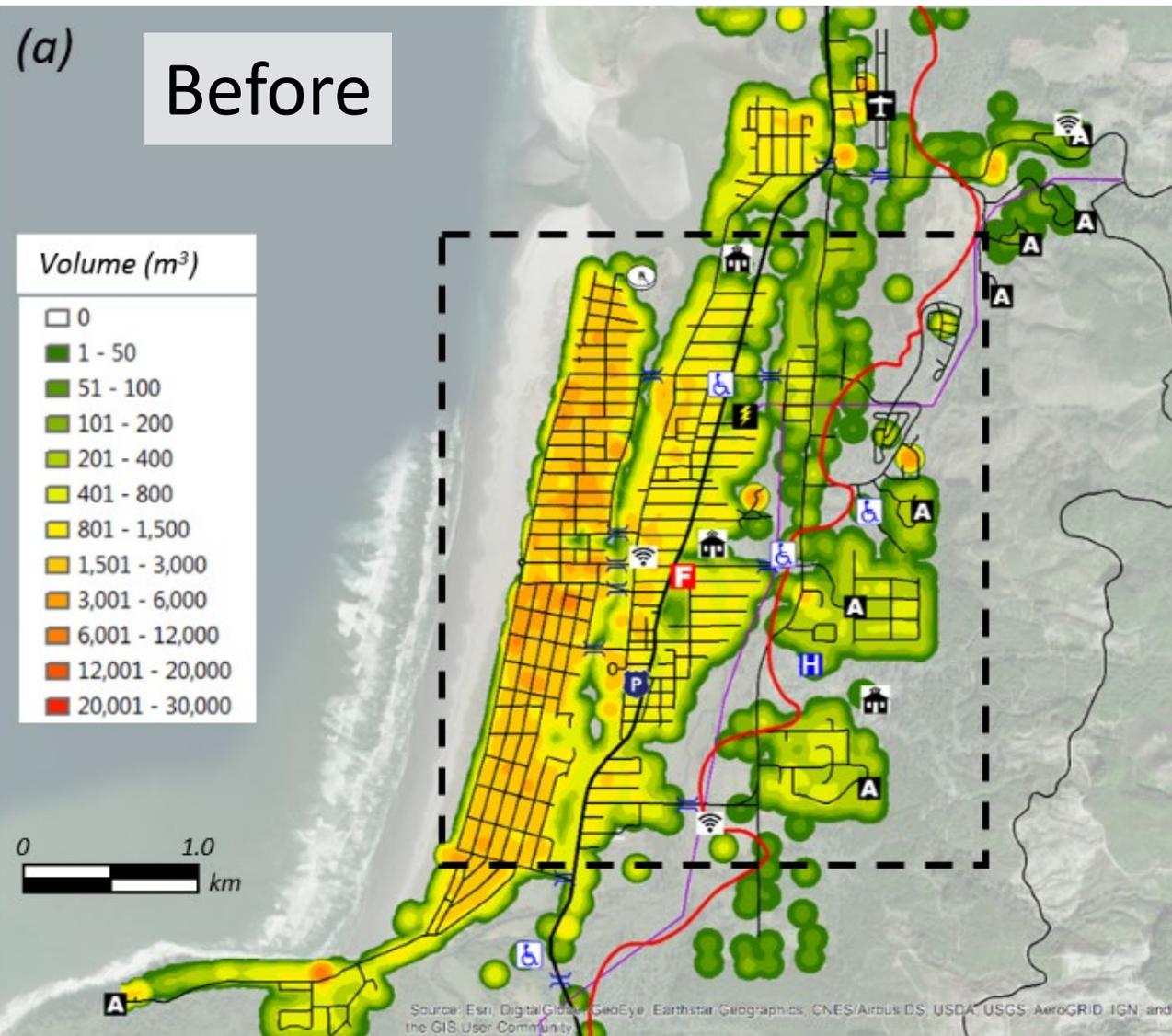
Advection of buoyant debris from PSTDA at AEP = 0.0004 (2,500 yr)



Thresholds: 3 m, 0.5 m/s

1 m, 0.3 m/s

0.5 m, 0.2 m/s



Park H, DT Cox (2019) "Effects of advection on forecasting construction debris for vulnerability assessment under multi-hazard earthquake and tsunami," *Coastal Engineering* <https://doi.org/10.1016/j.coastaleng.2019.103541>

Post-event Community Connectivity and Access to Critical Facilities

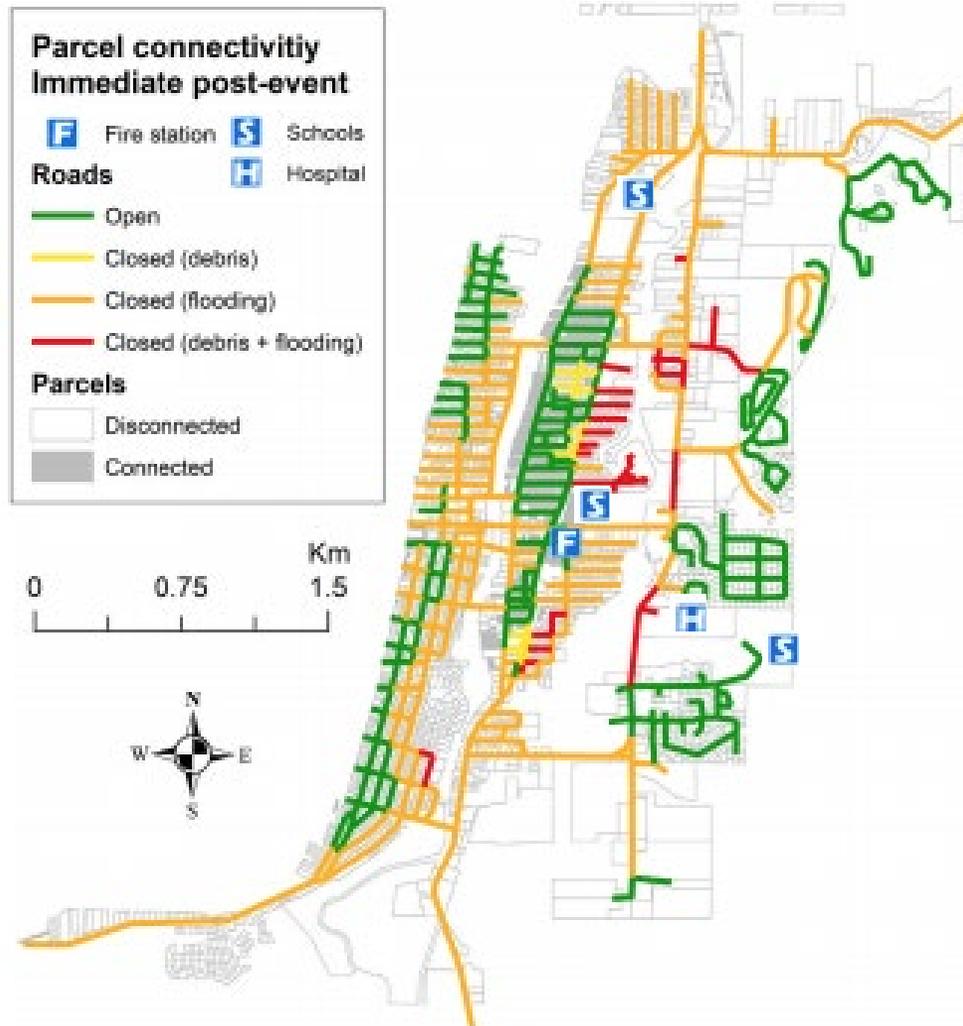


Table 1

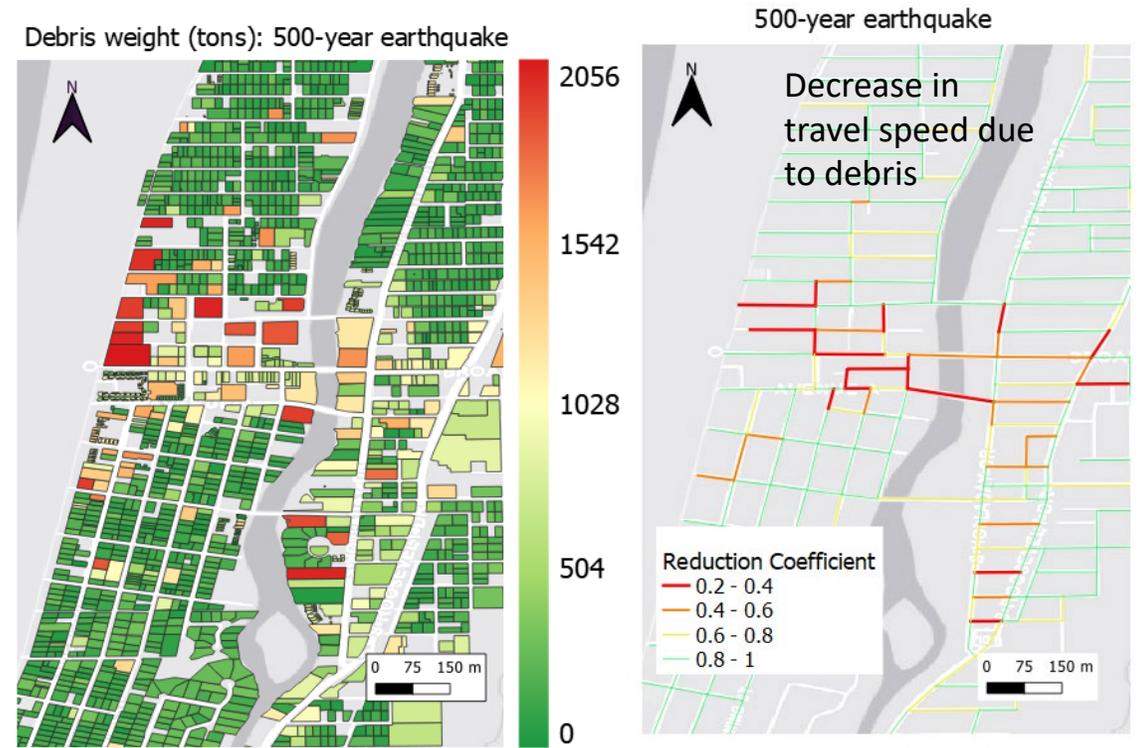
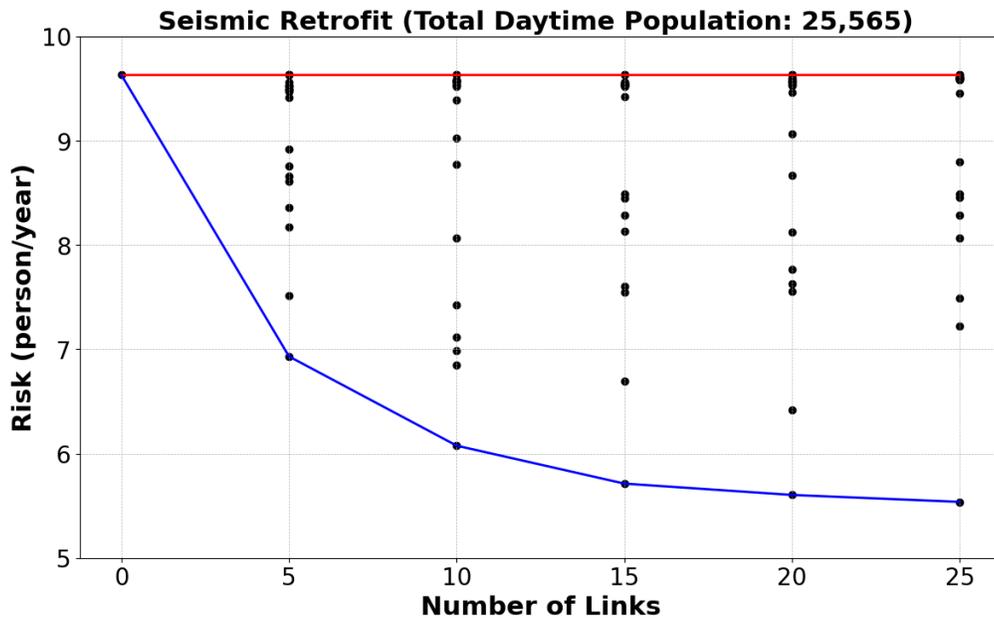
Likelihood of accessing hospitals and the high school immediately after tsunami events.

| (a) Connectivity to hospital | | | | | |
|-------------------------------------|-------|-------|-------|-------|-------|
| Return period | AA #2 | AA #5 | AA #6 | AA #7 | AA #8 |
| 250 | 0.84 | 1.00 | 1.00 | 1.00 | 0.99 |
| 500 | 0.67 | 1.00 | 1.00 | 1.00 | 0.82 |
| 1000 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 2500 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| 5000 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 10000 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

| (b) Connectivity to high school | | | | | |
|--|-------|-------|-------|-------|-------|
| Return period | AA #2 | AA #5 | AA #6 | AA #7 | AA #8 |
| 250 | 0.83 | 0.99 | 0.99 | 0.99 | 1.00 |
| 500 | 0.63 | 0.95 | 0.95 | 0.95 | 0.86 |
| 1000 | 0.10 | 0.00 | 0.34 | 0.02 | 0.32 |
| 2500 | 0.01 | 0.00 | 0.05 | 0.00 | 0.04 |
| 5000 | 0.00 | 0.00 | 0.00 | 0.00 | 0.04 |
| 10000 | 0.00 | 0.00 | 0.00 | 0.00 | 0.02 |

Life Safety Modeling

- Effect of earthquake damage on the tsunami casualty:
 - EQ damage increases building evacuation time.
 - EQ debris increases pedestrian evacuation time.
- Work in progress:
 - Risk-based modeling for EQ + Tsu
 - Inclusion of **tourist** in life safety and risk
 - Impact of **structural retrofit** on building egress and road debris



Thank you!

Dan Cox
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Center for Risk-Based Community Resilience Planning
A NIST-funded Center of Excellence